

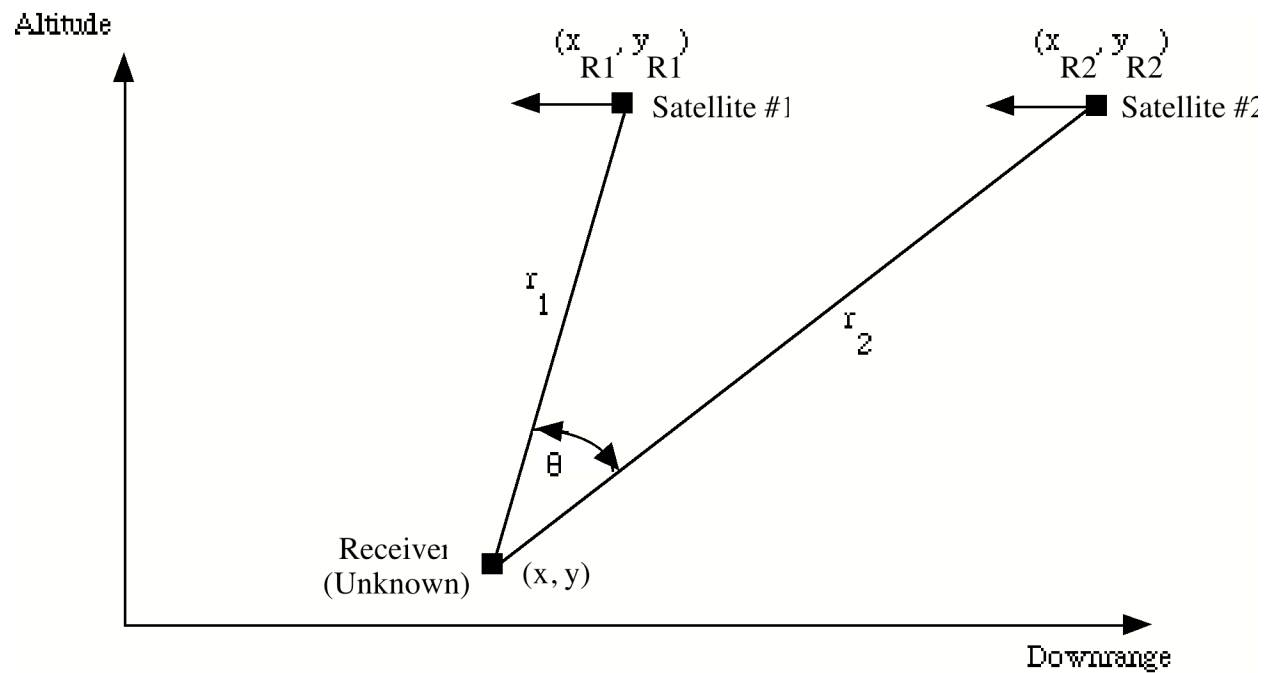
Biases

Biases Overview

- **Demonstration of problem**
- **Estimating satellite bias based on known receiver location**
- **Estimating receiver bias with unknown receiver location**
 - **2 satellites**
 - **3 satellites**

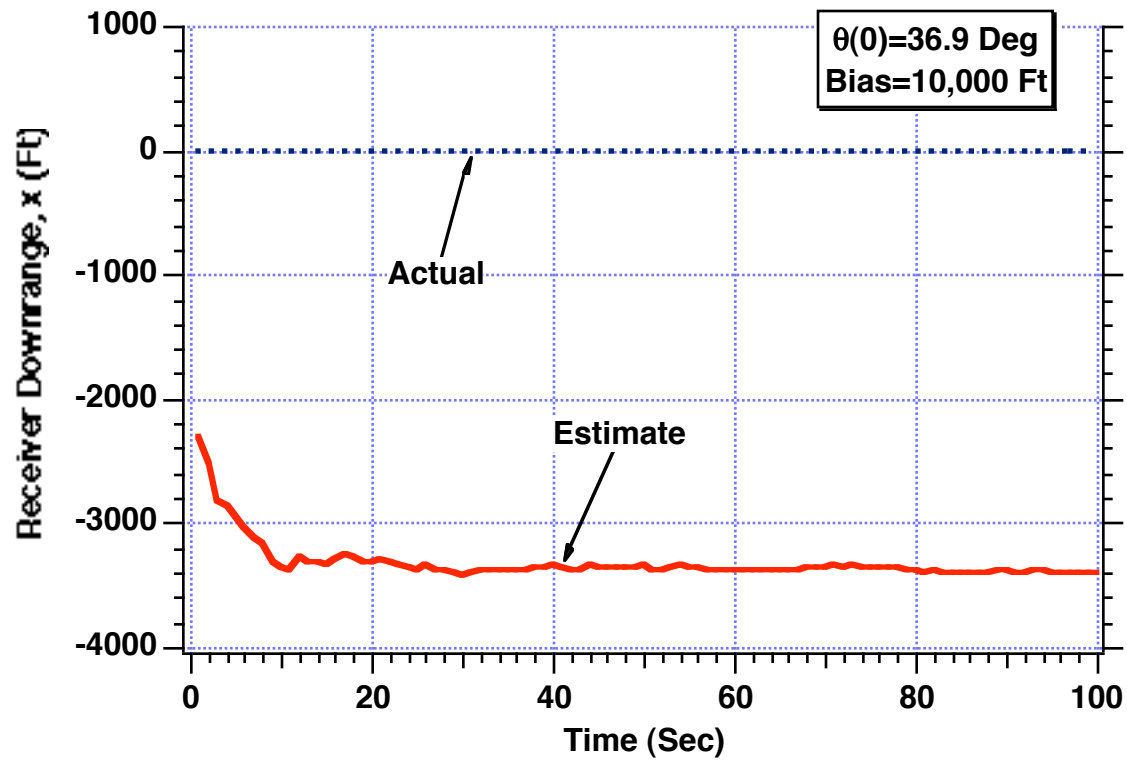
Demonstration of Problem

Satellite Geometry For Filtering Experiment

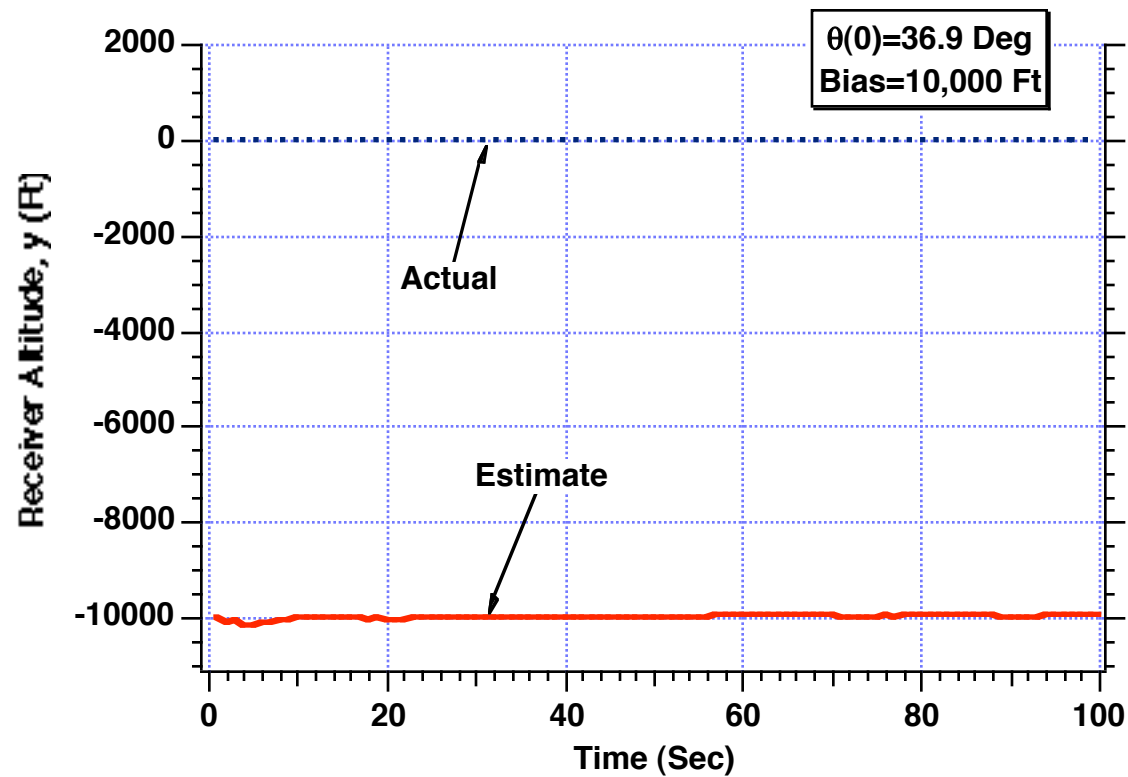


Range measurements have bias on them

Filter is Unable to Estimate Receiver Downrange When Range Bias is Present

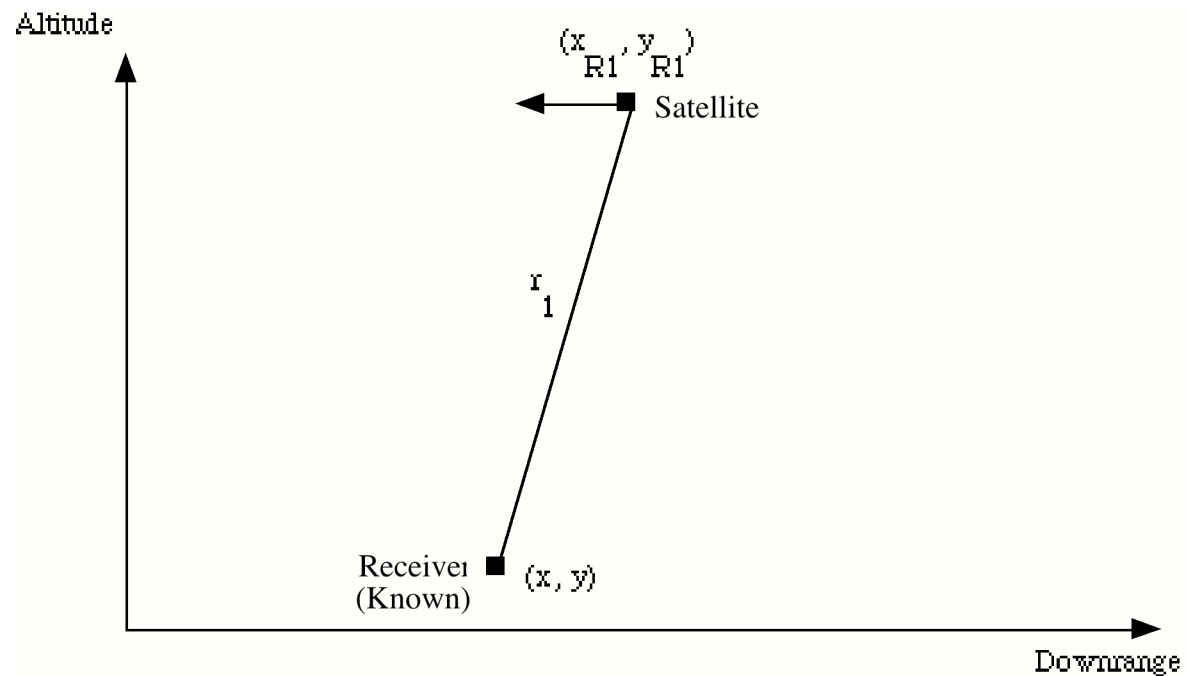


Filter is Unable to Estimate Receiver Altitude When Range Bias is Present



Estimating Satellite Bias With Known Receiver Location

Geometry for Attempting to Estimate Range Bias



Range measurement has bias on it

Estimating Bias on Range-1

Actual range from satellite to receiver

$$r_1 = \sqrt{(x_{R1} - x)^2 + (y_{R1} - y)^2}$$

Measured range

$$r_1^* = \sqrt{(x_{R1} - x)^2 + (y_{R1} - y)^2} + \text{BIAS} + v_{r1}$$

Discrete noise matrix is a scalar

$$R_k = \sigma_{r1}^2$$

State space equation for bias

$$\text{BIAS} = u_s$$

Systems dynamics matrix is zero therefore

$$\Phi_k = 1$$

Continuous process noise matrix is a scalar

$$Q = \Phi_s$$

Estimating Bias on Range-2

Formula for discrete process noise matrix

$$Q_k = \int_0^{T_s} \Phi(\tau) Q \Phi^T(\tau) d\tau$$

Substitution yields

$$Q_k = \int_0^{T_s} 1 * \Phi_s * 1 d\tau = \Phi_s T_s$$

Or

$$Q_k = \Phi_s T_s$$

Since measured range is

$$r_1^* = \sqrt{(x_{R1} - x)^2 + (y_{R1} - y)^2} + \text{BIAS} + v_{r1}$$

Linearized range measurement is

$$\Delta r_1^* = \frac{\partial r_1^*}{\partial \text{BIAS}} \Delta \text{BIAS} + v$$

Estimating Bias on Range-3

Partial derivative evaluated as

$$\frac{\partial r_1^*}{\partial \text{BIAS}} = 1$$

Therefore linearized measurement matrix is

$$\mathbf{H}_k = 1$$

Since fundamental matrix is unity projected bias is

$$\overline{\text{BIAS}}_k = \widehat{\text{BIAS}}_{k-1}$$

Projected range from satellite to receiver

$$\bar{r}_{1k} = \sqrt{(x_{R1k} - x_k)^2 + (y_{R1k} - y_k)^2} + \overline{\text{BIAS}}_k$$

Residual and filter

$$\text{RES}_k = r_{1k}^* - \bar{r}_{1k}$$

$$\widehat{\text{BIAS}}_k = \overline{\text{BIAS}}_k + K_{1k} \text{RES}_k$$

FORTRAN Extended Kalman Filter to Estimate Range Bias if Receiver Location is Known-1

```
GLOBAL DEFINE
      INCLUDE 'quickdraw.inc'
END
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
REAL*8 M,MHT,KH,IKH
INTEGER ORDER
SIGNOISE=300.
BIAS=10000.
BIASH=0.
X=0.
Y=0.
XR1=1000000.
YR1=20000.*3280.
OPEN(2,STATUS='UNKNOWN',FILE='COVFIL')
OPEN(1,STATUS='UNKNOWN',FILE='DATFIL')
ORDER=1
TS=1.
TF=100.
PHIS=0.
Q=PHIS*TS
T=0.
S=0.
H=.01
P=10000.**2
RMAT=SIGNOISE**2
WHILE(T<=TF)
      XR1OLD=XR1
      XR1D=-14600.
      XR1=XR1+H*XR1D
      T=T+H
      XR1D=-14600.
      XR1=.5*(XR1OLD+XR1+H*XR1D)
      S=S+H
```

Integrating satellite equations

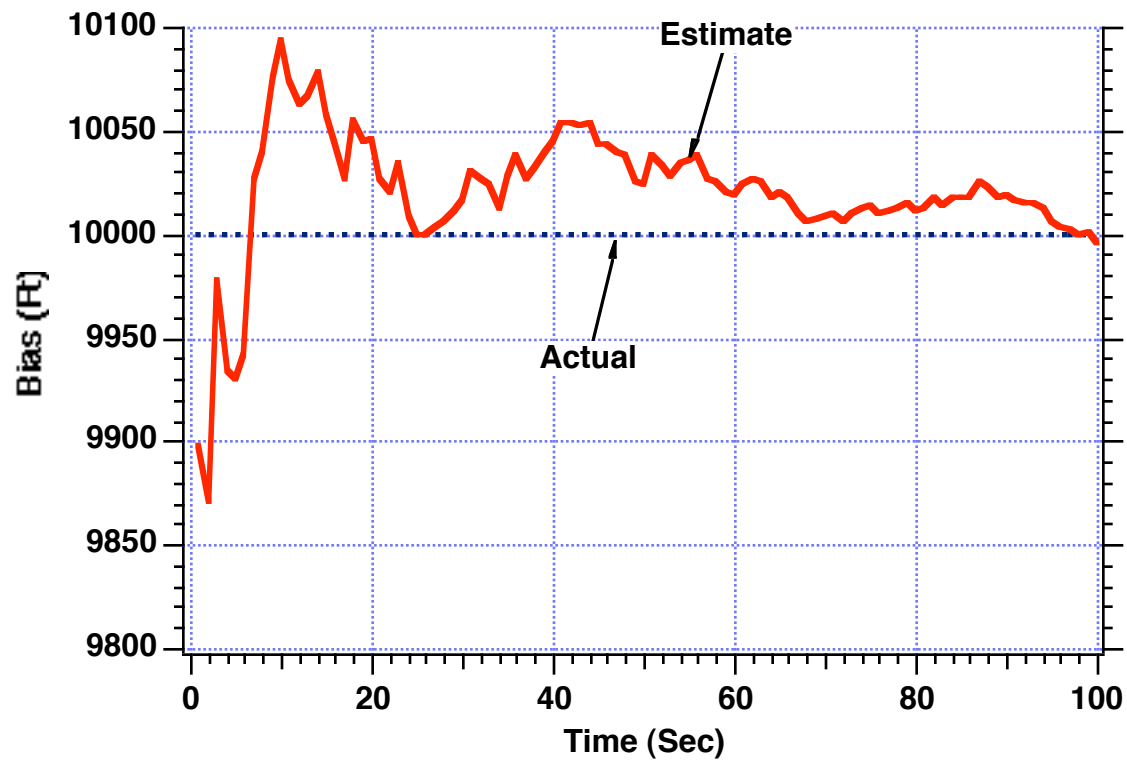
FORTRAN Extended Kalman Filter to Estimate Range Bias if Receiver Location is Known-2

```
IF(S>=(TS-.00001))THEN
  S=0.
  BIASB=BIASH
  R1B=SQRT((XR1-X)**2+(YR1-Y)**2)+BIASB
  R1H=SQRT((XR1-X)**2+(YR1-Y)**2)+BIASH
  HMAT=1.
  M=P+Q
  HMHT=HMAT*HMAT*M
  HMHTR=HMHT+RMAT
  HMHTRINV=1./HMHTR
  MHT=M*HMAT
  GAIN=MHT*HMHTRINV
  KH=GAIN*HMAT
  IKH=1.-KH
  P=IKH*M
  CALL GAUSS(R1NOISE,SIGNOISE)
  R1=SQRT((XR1-X)**2+(YR1-Y)**2)+BIAS
  RES1=R1+R1NOISE-R1H
  BIASH=BIASB+GAIN*RES1
  ERRBIAS=BIAS-BIASH
  SP11=SQRT(P)
  WRITE(9,*)T,BIAS,BIASH
  WRITE(1,*)T,BIAS,BIASH
  WRITE(2,*)T,ERRBIAS,SP11,-SP11
ENDIF
END DO
PAUSE
CLOSE(1)
CLOSE(2)
END
```

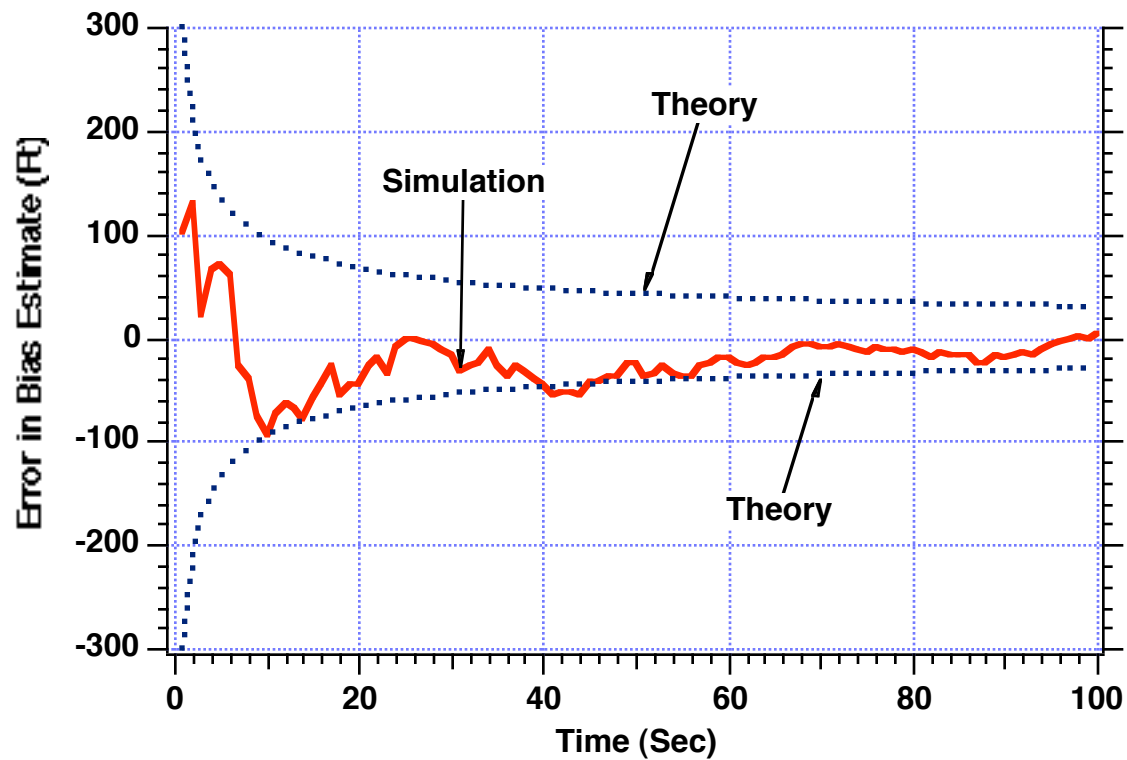
Scalar Riccati equations

Filter

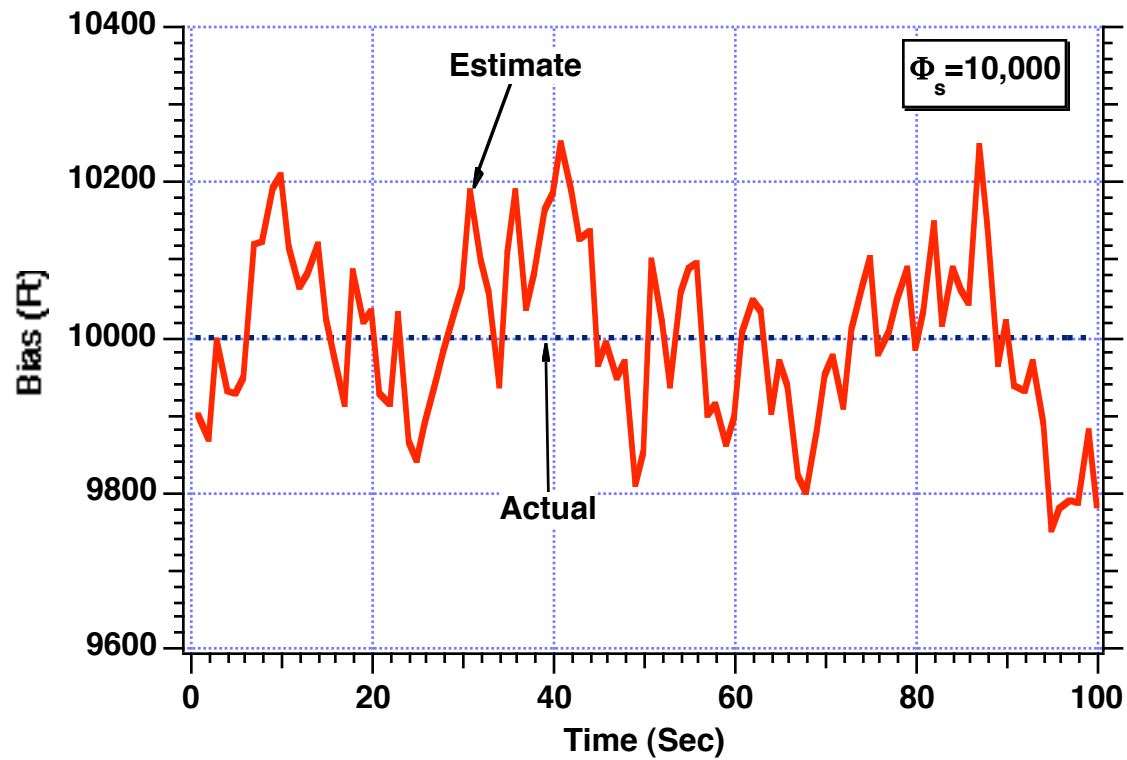
Bias Can be Estimated if Receiver Location is Known



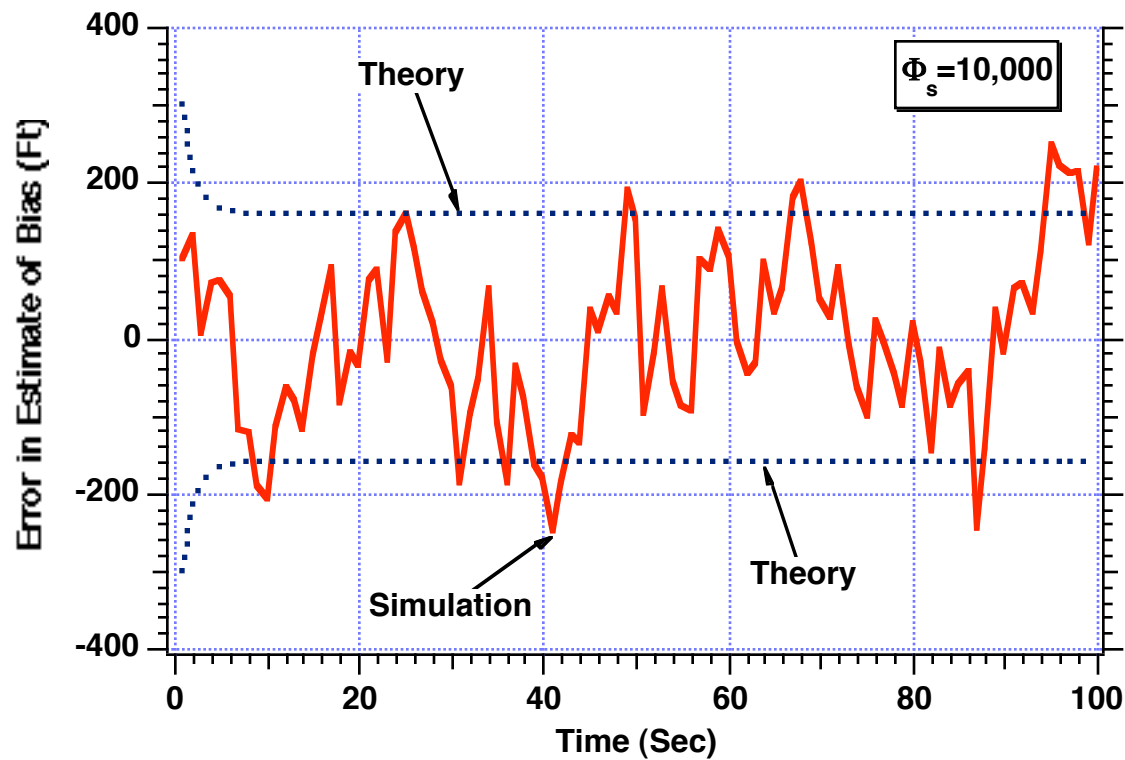
Extended Kalman Filter Appears to be Working Properly



Adding Process Noise Degrades Estimate of Bias

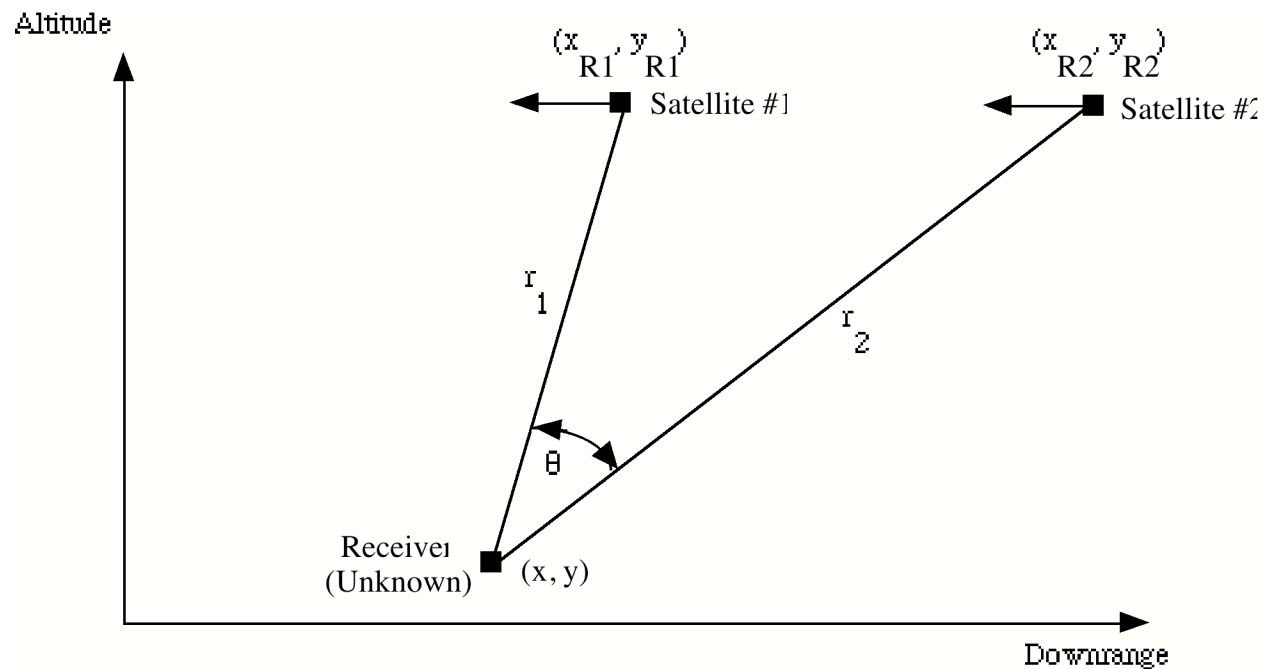


Adding Process Noise Causes Errors in Estimate of Bias to Approach a Steady State



Estimating Receiver Bias With Unknown Receiver Location and Two Satellites

Geometry for Estimating Receiver Location and Range Bias Due to the Receiver Based on Range Measurements From Two Satellites



Range measurements have bias on them

Designing Extended Kalman Filter-1

Model of real world for stationary receiver

$$\dot{x} = 0$$

$$\dot{y} = 0$$

$$\text{BIAS} = u_s$$

State space model

$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \text{BIAS} \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x \\ y \\ \text{BIAS} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ u_s \end{bmatrix}$$

Systems dynamics matrix is zero

$$\mathbf{F} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

Therefore fundamental matrix is identity matrix

$$\Phi_k = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Designing Extended Kalman Filter-2

Continuous process noise matrix

$$Q = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & \Phi_s \end{bmatrix}$$

Discrete process noise matrix

$$Q_k = \int_0^{T_s} \Phi(\tau) Q \Phi^T(\tau) d\tau \longrightarrow Q_k = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & \Phi_s T_s \end{bmatrix}$$

True range from each satellite to receiver

$$r_1 = \sqrt{(x_{R1} - x)^2 + (y_{R1} - y)^2}$$

$$r_2 = \sqrt{(x_{R2} - x)^2 + (y_{R2} - y)^2}$$

Measured range from each satellite

$$r_1^* = \sqrt{(x_{R1} - x)^2 + (y_{R1} - y)^2} + \text{BIAS} + v_{r1}$$

$$r_2^* = \sqrt{(x_{R2} - x)^2 + (y_{R2} - y)^2} + \text{BIAS} + v_{r2}$$

Designing Extended Kalman Filter-3

Linearized measurement equation

$$\begin{bmatrix} \Delta r_1^* \\ \Delta r_2^* \end{bmatrix} = \begin{bmatrix} \frac{\partial r_1^*}{\partial x} & \frac{\partial r_1^*}{\partial y} & \frac{\partial r_1^*}{\partial \text{BIAS}} \\ \frac{\partial r_2^*}{\partial x} & \frac{\partial r_2^*}{\partial y} & \frac{\partial r_2^*}{\partial \text{BIAS}} \end{bmatrix} \begin{bmatrix} \Delta x \\ \Delta y \\ \Delta \text{BIAS} \end{bmatrix} + \begin{bmatrix} v_{r1} \\ v_{r2} \end{bmatrix}$$

Discrete measurement noise matrix

$$\mathbf{R}_k = \begin{bmatrix} \sigma_{r1}^2 & 0 \\ 0 & \sigma_{r2}^2 \end{bmatrix}$$

Linearized measurement matrix

$$\mathbf{H}_k = \begin{bmatrix} \frac{\partial r_1^*}{\partial x} & \frac{\partial r_1^*}{\partial y} & \frac{\partial r_1^*}{\partial \text{BIAS}} \\ \frac{\partial r_2^*}{\partial x} & \frac{\partial r_2^*}{\partial y} & \frac{\partial r_2^*}{\partial \text{BIAS}} \end{bmatrix}$$

Designing Extended Kalman Filter-4

Evaluating partial derivatives

$$r_1^* = \sqrt{(x_{R1} - x)^2 + (y_{R1} - y)^2} + \text{BIAS} + v_{r1} \longrightarrow \frac{\partial r_1^*}{\partial x} = .5 [(x_{R1}-x)^2+(y_{R1}-y)^2]^{-.5} 2(x_{R1}-x)(-1) = \frac{-(x_{R1}-x)}{r_1}$$

$$\frac{\partial r_1^*}{\partial y} = .5 [(x_{R1}-x)^2+(y_{R1}-y)^2]^{-.5} 2(y_{R1}-y)(-1) = \frac{-(y_{R1}-y)}{r_1}$$

$$\frac{\partial r_1^*}{\partial \text{BIAS}} = 1$$

$$r_2^* = \sqrt{(x_{R2} - x)^2 + (y_{R2} - y)^2} + \text{BIAS} + v_{r2} \longrightarrow \frac{\partial r_2^*}{\partial x} = .5 [(x_{R1}-x)^2+(y_{R1}-y)^2]^{-.5} 2(x_{R2}-x)(-1) = \frac{-(x_{R2}-x)}{r_2}$$

$$\frac{\partial r_2^*}{\partial y} = .5 [(x_{R1}-x)^2+(y_{R1}-y)^2]^{-.5} 2(y_{R2}-y)(-1) = \frac{-(y_{R2}-y)}{r_2}$$

$$\frac{\partial r_2^*}{\partial \text{BIAS}} = 1$$

Linearized measurement matrix

$$\mathbf{H}_k = \begin{bmatrix} \frac{-(x_{R1}-x)}{r_1} & \frac{-(y_{R1}-y)}{r_1} & 1 \\ \frac{-(x_{R2}-x)}{r_2} & \frac{-(y_{R2}-y)}{r_2} & 1 \end{bmatrix}$$

Designing Extended Kalman Filter-5

Projected state estimates

$$\bar{x}_k = \hat{x}_{k-1}$$

$$\bar{y}_k = \hat{y}_{k-1}$$

$$\overline{\text{BIAS}}_k = \widehat{\text{BIAS}}_{k-1}$$

Projected ranges from each satellite

$$\bar{r}_{1k} = \sqrt{(x_{R1k} - \bar{x}_k)^2 + (y_{R1k} - \bar{y}_k)^2} + \overline{\text{BIAS}}_k$$

$$\bar{r}_{2k} = \sqrt{(x_{R2k} - \bar{x}_k)^2 + (y_{R2k} - \bar{y}_k)^2} + \overline{\text{BIAS}}_k$$

Filtering equations

$$\text{RES}_{1k} = r_{1k}^* - \bar{r}_{1k}$$

$$\text{RES}_{2k} = r_{2k}^* - \bar{r}_{2k}$$

$$\hat{x}_k = \bar{x}_k + K_{11k}\text{RES}_{1k} + K_{12k}\text{RES}_{2k}$$

$$\hat{y}_k = \bar{y}_k + K_{21k}\text{RES}_{1k} + K_{22k}\text{RES}_{2k}$$

$$\widehat{\text{BIAS}}_k = \overline{\text{BIAS}}_k + K_{31k}\text{RES}_{1k} + K_{32k}\text{RES}_{2k}$$

MATLAB Version of Extended Kalman Filter-1

```
SIGNOISE=300.;
```

```
TF=100.;
```

```
X=0.;
```

```
Y=0.;
```

```
XH=1000.;
```

```
YH=2000.;
```

```
XR1=1000000.;
```

```
YR1=20000.*3280.;
```

```
XR2=50000000.;
```

```
YR2=20000.*3280.;
```

```
BIAS=10000.;
```

```
BIASH=0.;
```

```
PHIS=0.;
```

```
ORDER=3;
```

```
TS=1.;
```

```
T=0.;
```

```
S=0.;
```

```
H=.01;
```

```
PHI=zeros(ORDER,ORDER);
```

```
P=zeros(ORDER,ORDER);
```

```
IDNP=eye(ORDER);
```

```
Q=zeros(ORDER,ORDER);
```

```
Q(3,3)=PHIS*TS;
```

```
P(1,1)=1000.^2;
```

```
P(2,2)=2000.^2;
```

```
P(3,3)=500.^2;
```

```
RMAT(1,1)=SIGNOISE^2;
```

```
RMAT(1,2)=0.;
```

```
RMAT(2,1)=0.;
```

```
RMAT(2,2)=SIGNOISE^2;
```

```
count=0;
```

Actual and estimated receiver location

Actual and estimated range bias

Initial covariance matrix

Measurement noise matrix

MATLAB Version of Extended Kalman Filter-2

while T<=TF

```

XR1OLD=XR1;
XR2OLD=XR2;
XR1D=-14600.;
XR2D=-14600.;
XR1=XR1+H*XR1D;
XR2=XR2+H*XR2D;
T=T+H;
XR1D=-14600.;
XR2D=-14600.;
XR1=.5*(XR1OLD+XR1+H*XR1D);
XR2=.5*(XR2OLD+XR2+H*XR2D);
S=S+H;
if S>=(TS-.00001)

```

Integration of satellite equations with second-order Runge-Kutta technique

```

S=0.;
R1H=sqrt((XR1-XH)^2+(YR1-YH)^2)+BIASH;
R2H=sqrt((XR2-XH)^2+(YR2-YH)^2)+BIASH;
HMAT(1,1)=(XR1-XH)/sqrt((XR1-XH)^2+(YR1-YH)^2);
HMAT(1,2)=(YR1-YH)/sqrt((XR1-XH)^2+(YR1-YH)^2);
HMAT(1,3)=1.;
HMAT(2,1)=(XR2-XH)/sqrt((XR2-XH)^2+(YR2-YH)^2);
HMAT(2,2)=(YR2-YH)/sqrt((XR2-XH)^2+(YR2-YH)^2);
HMAT(2,3)=1.;
HT=HMAT';

```

Linearized measurement matrix

```

PHI(1,1)=1.;
PHI(2,2)=1.;
PHI(3,3)=1.;
PHIT=PHI';

```

Fundamental matrix

```

PHIP=PHI*P;
PHIPPHIT=PHIP*PHIT;
M=PHIPPHIT+Q;
HM=HMAT*M;
HMHT=HM*HT;
HMHTR=HMHT+RMAT;
HMHTRINV=inv(HMHTR);
MHT=M*HT;
GAIN=MHT*HMHTRINV;
KH=GAIN*HMAT;
IKH=IDNP-KH;
P=IKH*M;

```

Riccati equations

MATLAB Version of Extended Kalman Filter-3

```
R1NOISE=SIGNOISE*randn;
R2NOISE=SIGNOISE*randn;
R1=sqrt((XR1-X)^2+(YR1-Y)^2);
R2=sqrt((XR2-X)^2+(YR2-Y)^2);
RES1=R1+R1NOISE+BIAS-R1H;
RES2=R2+R2NOISE+BIAS-R2H;
XH=XH+GAIN(1,1)*RES1+GAIN(1,2)*RES2;
YH=YH+GAIN(2,1)*RES1+GAIN(2,2)*RES2;
BIASH=BIASH+GAIN(3,1)*RES1+GAIN(3,2)*RES2;
ERRX=X-XH;
SP11=sqrt(P(1,1));
ERRY=Y-YH;
SP22=sqrt(P(2,2));
ERRBIAS=BIAS-BIASH;
SP33=sqrt(P(3,3));
R1T=sqrt((XR1-X)^2+(YR1-Y)^2);
R2T=sqrt((XR2-X)^2+(YR2-Y)^2);
TEMP=(XR1-X)*(XR2-X)+(YR1-Y)*(YR2-Y);
TH=atan2(sqrt((R1T*R2T)^2-TEMP^2),TEMP);
THET=57.3*TH;
SP11P=SP11;
SP22P=SP22;
SP33P=SP33;
count=count+1;
ArrayT(count)=T;
ArrayX(count)=X;
ArrayXH(count)=XH;
ArrayY(count)=Y;
ArrayYH(count)=YH;
ArrayBIAS(count)=BIAS;
ArrayBIASH(count)=BIASH;
ArrayERRX(count)=ERRX;
ArraySP11(count)=SP11;
ArraySP11P(count)=SP11P;
ArrayERRY(count)=ERRY;
ArraySP22(count)=SP22;
ArraySP22P(count)=SP22P;
ArrayERRBIAS(count)=ERRBIAS;
ArraySP33(count)=SP33;
ArraySP33P(count)=SP33P;
```

end

end

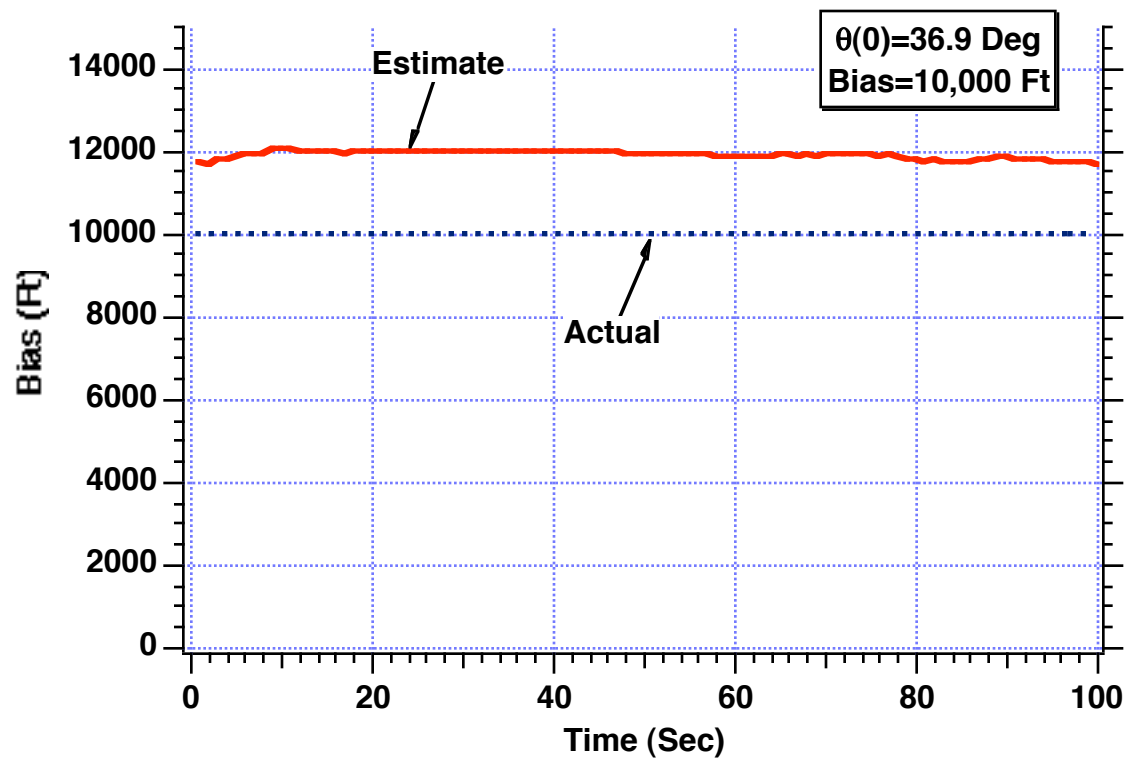
Filter

Actual and theoretical
errors in estimates

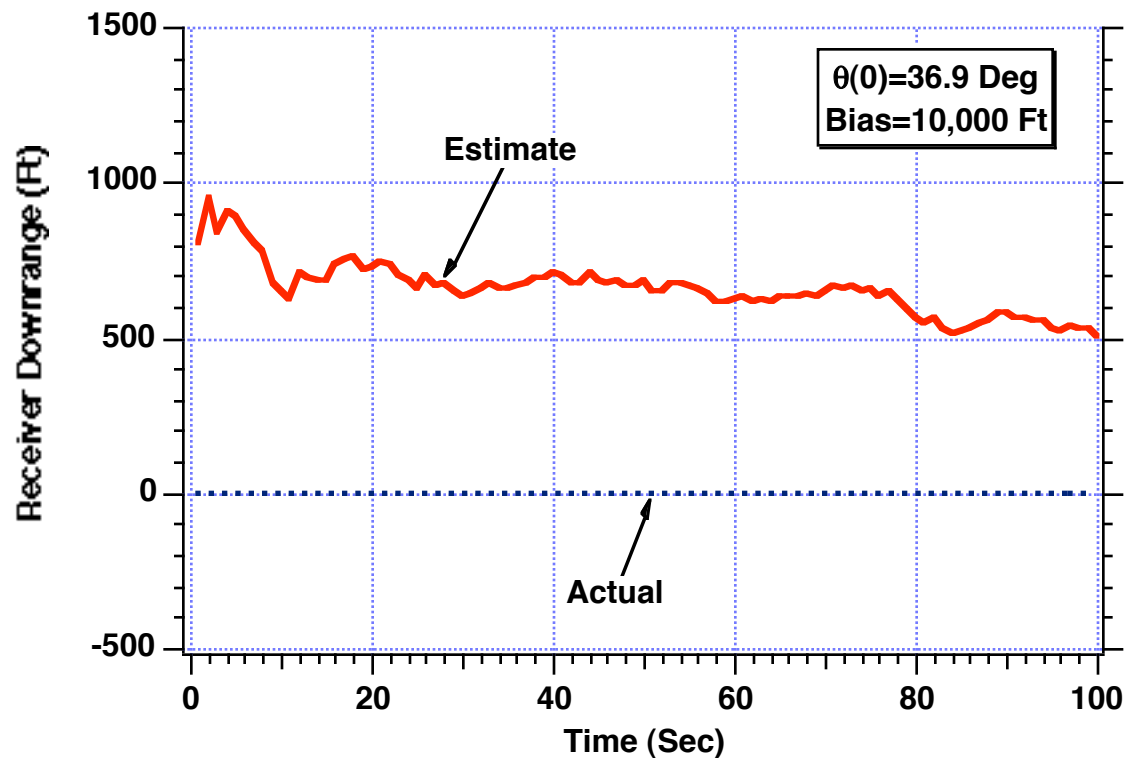
Angle between two range vectors

Save data as arrays for plotting
and writing to files

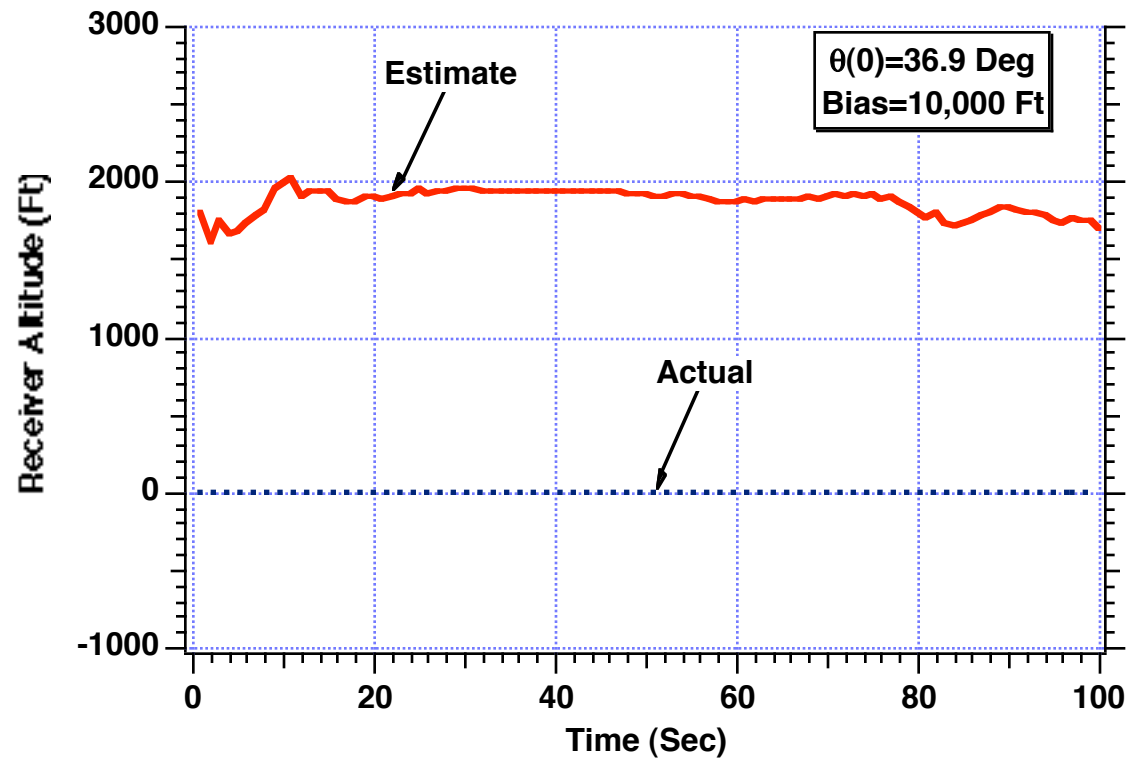
Extended Kalman Filter is Unable to Estimate Bias Based on Range Measurements From Two Satellites



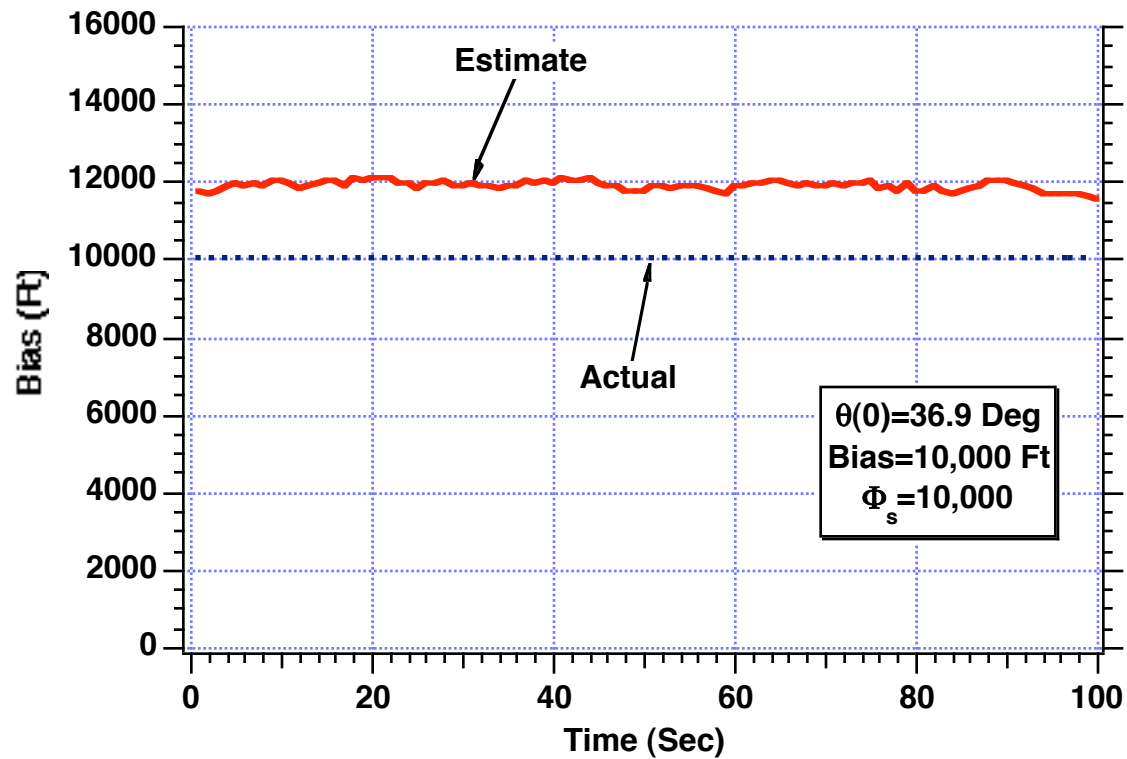
Extended Kalman Filter is Unable to Estimate Receiver Downrange Based on Range Measurements From Two Satellites



Extended Kalman Filter is Unable to Estimate Receiver Altitude Based on Range Measurements From Two Satellites

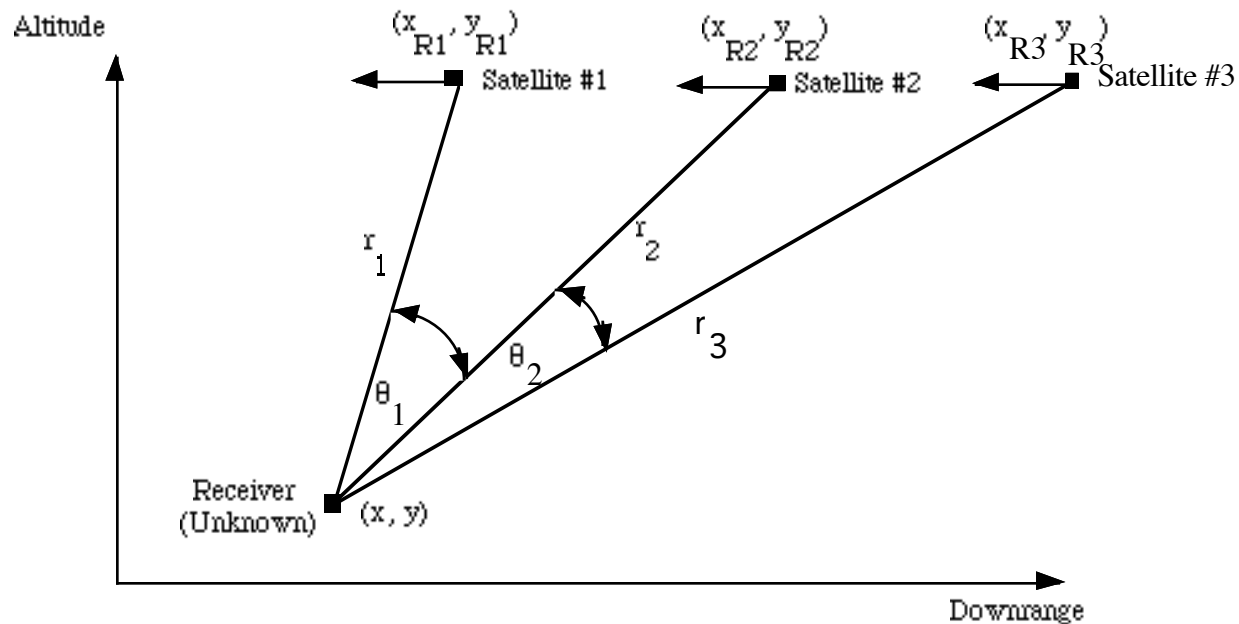


Process Noise Does Not Help Filter to Estimate Bias



Estimating Receiver Bias With Unknown Receiver Location and Three Satellites

Geometry for Estimating Receiver Location and Range Bias Based on Range Measurements From Three Satellites



Range measurements have bias in them

Designing Extended New Kalman Filter-1

Model of real world for stationary receiver

$$\dot{x} = 0$$

$$\dot{y} = 0$$

$$\text{BIAS} = u_s$$

State space model

$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \text{BIAS} \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x \\ y \\ \text{BIAS} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ u_s \end{bmatrix}$$

Systems dynamics matrix is zero

$$\mathbf{F} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

Therefore fundamental matrix is identity matrix

$$\Phi_k = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Designing New Extended Kalman Filter-2

Continuous process noise matrix

$$Q = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & \Phi_s \end{bmatrix}$$

Discrete process noise matrix

$$Q_k = \int_0^{T_s} \Phi(\tau) Q \Phi^T(\tau) d\tau \longrightarrow Q_k = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & \Phi_s T_s \end{bmatrix}$$

True range from each satellite to receiver

$$r_1 = \sqrt{(x_{R1} - x)^2 + (y_{R1} - y)^2}$$

$$r_2 = \sqrt{(x_{R2} - x)^2 + (y_{R2} - y)^2}$$

$$r_3 = \sqrt{(x_{R3} - x)^2 + (y_{R3} - y)^2}$$

Measured range from each satellite

$$r_1^* = \sqrt{(x_{R1} - x)^2 + (y_{R1} - y)^2} + \text{BIAS} + v_{r1}$$

$$r_2^* = \sqrt{(x_{R2} - x)^2 + (y_{R2} - y)^2} + \text{BIAS} + v_{r2}$$

$$r_3^* = \sqrt{(x_{R3} - x)^2 + (y_{R3} - y)^2} + \text{BIAS} + v_{r3}$$

Designing New Extended Kalman Filter-3

Linearized measurement equation

$$\begin{bmatrix} \Delta r_1^* \\ \Delta r_2^* \\ \Delta r_3^* \end{bmatrix} = \begin{bmatrix} \frac{\partial r_1^*}{\partial x} & \frac{\partial r_1^*}{\partial y} & \frac{\partial r_1^*}{\partial \text{BIAS}} \\ \frac{\partial r_2^*}{\partial x} & \frac{\partial r_2^*}{\partial y} & \frac{\partial r_2^*}{\partial \text{BIAS}} \\ \frac{\partial r_3^*}{\partial x} & \frac{\partial r_3^*}{\partial y} & \frac{\partial r_3^*}{\partial \text{BIAS}} \end{bmatrix} \begin{bmatrix} \Delta x \\ \Delta y \\ \Delta \text{BIAS} \end{bmatrix} + \begin{bmatrix} v_{r1} \\ v_{r2} \\ v_{r3} \end{bmatrix}$$

Discrete measurement noise matrix

$$\mathbf{R}_k = \begin{bmatrix} \sigma_{r1}^2 & 0 & 0 \\ 0 & \sigma_{r2}^2 & 0 \\ 0 & 0 & \sigma_{r3}^2 \end{bmatrix}$$

Linearized measurement matrix

$$\mathbf{H}_k = \begin{bmatrix} \frac{\partial r_1^*}{\partial x} & \frac{\partial r_1^*}{\partial y} & \frac{\partial r_1^*}{\partial \text{BIAS}} \\ \frac{\partial r_2^*}{\partial x} & \frac{\partial r_2^*}{\partial y} & \frac{\partial r_2^*}{\partial \text{BIAS}} \\ \frac{\partial r_3^*}{\partial x} & \frac{\partial r_3^*}{\partial y} & \frac{\partial r_3^*}{\partial \text{BIAS}} \end{bmatrix}$$

Designing New Extended Kalman Filter-4

Evaluating partial derivatives

$$r_1^* = \sqrt{(x_{R1} - x)^2 + (y_{R1} - y)^2} + \text{BIAS} + v_{r1} \longrightarrow \frac{\partial r_1^*}{\partial x} = .5 [(x_{R1}-x)^2+(y_{R1}-y)^2]^{-.5} 2(x_{R1}-x)(-1) = \frac{-(x_{R1}-x)}{r_1}$$

$$\frac{\partial r_1^*}{\partial y} = .5 [(x_{R1}-x)^2+(y_{R1}-y)^2]^{-.5} 2(y_{R1}-y)(-1) = \frac{-(y_{R1}-y)}{r_1}$$

$$\frac{\partial r_1^*}{\partial \text{BIAS}} = 1$$

$$r_2^* = \sqrt{(x_{R2} - x)^2 + (y_{R2} - y)^2} + \text{BIAS} + v_{r2} \longrightarrow \frac{\partial r_2^*}{\partial x} = .5 [(x_{R1}-x)^2+(y_{R1}-y)^2]^{-.5} 2(x_{R2}-x)(-1) = \frac{-(x_{R2}-x)}{r_2}$$

$$\frac{\partial r_2^*}{\partial y} = .5 [(x_{R1}-x)^2+(y_{R1}-y)^2]^{-.5} 2(y_{R2}-y)(-1) = \frac{-(y_{R2}-y)}{r_2}$$

$$\frac{\partial r_2^*}{\partial \text{BIAS}} = 1$$

$$r_3^* = \sqrt{(x_{R3} - x)^2 + (y_{R3} - y)^2} + \text{BIAS} + v_{r3} \longrightarrow \frac{\partial r_3^*}{\partial x} = .5 [(x_{R3}-x)^2+(y_{R3}-y)^2]^{-.5} 2(x_{R3}-x)(-1) = \frac{-(x_{R3}-x)}{r_3}$$

$$\frac{\partial r_3^*}{\partial y} = .5 [(x_{R3}-x)^2+(y_{R3}-y)^2]^{-.5} 2(y_{R3}-y)(-1) = \frac{-(y_{R3}-y)}{r_3}$$

$$\frac{\partial r_3^*}{\partial \text{BIAS}} = 1$$

Designing New Extended Kalman Filter-5

Linearized measurement matrix

$$\mathbf{H}_k = \begin{bmatrix} \frac{-(x_{R1}-x)}{r_1} & \frac{-(y_{R1}-y)}{r_1} & 1 \\ \frac{-(x_{R2}-x)}{r_2} & \frac{-(y_{R2}-y)}{r_2} & 1 \\ \frac{-(x_{R3}-x)}{r_3} & \frac{-(y_{R2}-y)}{r_2} & 1 \end{bmatrix}$$

Projected state estimates

$$\bar{x}_k = \hat{x}_{k-1}$$

$$\bar{y}_k = \hat{y}_{k-1}$$

$$\overline{\text{BIAS}}_k = \widehat{\text{BIAS}}_{k-1}$$

Projected ranges from each satellite

$$\bar{r}_{1k} = \sqrt{(x_{R1k} - \bar{x}_k)^2 + (y_{R1k} - \bar{y}_k)^2} + \overline{\text{BIAS}}_k$$

$$\bar{r}_{2k} = \sqrt{(x_{R2k} - \bar{x}_k)^2 + (y_{R2k} - \bar{y}_k)^2} + \overline{\text{BIAS}}_k$$

$$\bar{r}_{3k} = \sqrt{(x_{R3k} - \bar{x}_k)^2 + (y_{R3k} - \bar{y}_k)^2} + \overline{\text{BIAS}}_k$$

Designing Extended Kalman Filter-6

Filtering equations

$$\text{RES}_{1k} = r_{1k}^* - \bar{r}_{1k}$$

$$\text{RES}_{2k} = r_{2k}^* - \bar{r}_{2k}$$

$$\text{RES}_{3k} = r_{3k}^* - \bar{r}_{3k}$$

$$\hat{x}_k = \bar{x}_k + K_{11k}\text{RES}_{1k} + K_{12k}\text{RES}_{2k} + K_{13k}\text{RES}_{3k}$$

$$\hat{y}_k = \bar{y}_k + K_{21k}\text{RES}_{1k} + K_{22k}\text{RES}_{2k} + K_{23k}\text{RES}_{3k}$$

$$\widehat{\text{BIAS}}_k = \overline{\text{BIAS}}_k + K_{31k}\text{RES}_{1k} + K_{32k}\text{RES}_{2k} + K_{33k}\text{RES}_{3k}$$

True BASIC Version of New Extended Kalman Filter-1

```
OPTION NOLET
REM UNSAVE "DATFIL"
REM UNSAVE "COVFIL"
OPEN #1:NAME "DATFIL",ACCESS OUTPUT,CREATE NEW, ORGANIZATION TEXT
OPEN #2:NAME "COVFIL",ACCESS OUTPUT,CREATE NEW, ORGANIZATION TEXT
SET #1: MARGIN 1000
SET #2: MARGIN 1000
DIM PHI(3,3),P(3,3),M(3,3),PHIP(3,3),PHIPPHIT(3,3),GAIN(3,3)
DIM Q(3,3),HMAT(3,3),HM(3,3),MHT(3,3)
DIM PHIT(3,3),RMAT(3,3),HMHTRINV(3,3)
DIM HMHT(3,3),HT(3,3),KH(3,3),IDNP(3,3),IKH(3,3),HMHTR(3,3)
TF=100.
SIGNOISE=300.
X=0.
Y=0.
XH=1000.
YH=2000.
XR1=1000000.
YR1=20000.*3280.
XR2=50000000.
YR2=20000.*3280.
XR3=1000000000.
YR3=20000.*3280.
BIAS=10000.
BIASH=0.
PHIS=0.
ORDER=3
TS=1.
T=0.
S=0.
H=.01
MAT PHI=ZER(ORDER,ORDER)
MAT P=ZER(ORDER,ORDER)
MAT Q=ZER(ORDER,ORDER)
MAT IDNP=IDN(ORDER)
MAT RMAT=ZER(3,3)
Q(3,3)=PHIS*TS
```

Actual and estimated receiver location

Actual and estimated range bias

True BASIC Version of New Extended Kalman Filter-2

```

P(1,1)=1000.^2
P(2,2)=2000.^2
P(3,3)=(BIAS-BIASH)^2
RMAT(1,1)=SIGNOISE^2
RMAT(2,2)=SIGNOISE^2
RMAT(3,3)=SIGNOISE^2
DO WHILE T<=TF

```

Initial covariance matrix

Measurement noise matrix

```

XR1OLD=XR1
XR2OLD=XR2
XR3OLD=XR3
XR1D=-14600.
XR2D=-14600.
XR3D=-14600.
XR1=XR1+H*XR1D
XR2=XR2+H*XR2D
XR3=XR3+H*XR3D
T=T+H
XR1D=-14600.
XR2D=-14600.
XR3D=-14600.
XR1=.5*(XR1OLD+XR1+H*XR1D)
XR2=.5*(XR2OLD+XR2+H*XR2D)
XR3=.5*(XR3OLD+XR3+H*XR3D)
S=S+H
IF S>=(TS-.00001) THEN

```

Numerical integration of satellite equations with second-order Runge-Kutta technique

```

S=0.
R1H=SQR((XR1-XH)^2+(YR1-YH)^2)+BIASH
R2H=SQR((XR2-XH)^2+(YR2-YH)^2)+BIASH
R3H=SQR((XR3-XH)^2+(YR3-YH)^2)+BIASH
HMAT(1,1)=(XR1-XH)/SQR((XR1-XH)^2+(YR1-YH)^2)
HMAT(1,2)=(YR1-YH)/SQR((XR1-XH)^2+(YR1-YH)^2)
HMAT(1,3)=1.
HMAT(2,1)=(XR2-XH)/SQR((XR2-XH)^2+(YR2-YH)^2)
HMAT(2,2)=(YR2-YH)/SQR((XR2-XH)^2+(YR2-YH)^2)
HMAT(2,3)=1.
HMAT(3,1)=(XR3-XH)/SQR((XR3-XH)^2+(YR3-YH)^2)
HMAT(3,2)=(YR3-YH)/SQR((XR3-XH)^2+(YR3-YH)^2)
HMAT(3,3)=1.
MAT HT=TRN(HMAT)

```

Linearized measurement matrix

True BASIC Version of New Extended Kalman Filter-3

```
PHI(1,1)=1.
PHI(2,2)=1.
PHI(3,3)=1. ] Fundamental matrix
```

```
MAT PHIT=TRN(PHI)
MAT PHIP=PHI*P
MAT PHIPPHIT=PHIP*PHIT
MAT M=PHIPPHIT+Q
MAT HM=HMAT*M
MAT HMHT=HM*HT
MAT HMHTR=HMHT+RMAT
MAT HMHTRINV=INV(HMHTR)
MAT MHT=M*HT
MAT GAIN=MHT*HMHTRINV
MAT KH=GAIN*HMAT
MAT IKH=IDNP-KH
MAT P=IKH*M ] Riccati equations
```

```
CALL GAUSS(R1NOISE,SIGNOISE)
CALL GAUSS(R2NOISE,SIGNOISE)
CALL GAUSS(R3NOISE,SIGNOISE)
R1=SQR((XR1-X)^2+(YR1-Y)^2)
R2=SQR((XR2-X)^2+(YR2-Y)^2)
R3=SQR((XR3-X)^2+(YR3-Y)^2)
RES1=R1+R1NOISE+BIAS-R1H
RES2=R2+R2NOISE+BIAS-R2H
RES3=R3+R3NOISE+BIAS-R3H
XH=XH+GAIN(1,1)*RES1+GAIN(1,2)*RES2+GAIN(1,3)*RES3
YH=YH+GAIN(2,1)*RES1+GAIN(2,2)*RES2+GAIN(2,3)*RES3
BIASH=BIASH+GAIN(3,1)*RES1+GAIN(3,2)*RES2+GAIN(3,3)*RES3 ] Filter
```

```
ERRX=X-XH
SP11=SQR(P(1,1))
ERRY=Y-YH
SP22=SQR(P(2,2))
ERRBIAS=BIAS-BIASH
SP33=SQR(P(3,3)) ] Actual and theoretical errors in estimates
```

```
R1T=SQR((XR1-X)^2+(YR1-Y)^2)
R2T=SQR((XR2-X)^2+(YR2-Y)^2)
TEMP=(XR1-X)*(XR2-X)+(YR1-Y)*(YR2-Y)
CALL ATAN2(SQR((R1T*R2T)^2-TEMP^2), TEMP, TH1)
THET1=57.3*TH1
```

True BASIC Version of New Extended Kalman Filter-4

```
R3T=SQR((XR3-X)^2+(YR3-Y)^2)
TEMP3=(XR2-X)*(XR3-X)+(YR2-Y)*(YR3-Y)
CALL ATAN2(SQR((R2T*R3T)^2-TEMP3^2), TEMP3, TH2)
THET2=57.3*TH2
PRINT T,X,XH,Y,YH,BIAS,BIASH,THET1,THET2
PRINT #1:T,X,XH,Y,YH,BIAS,BIASH,THET1,THET2
PRINT #2:T,ERRX,SP11,-SP11,ERRY,SP22,-SP22,ERRBIAS,SP33,-SP33
```

END IF

```
LOOP
CLOSE #1
CLOSE #2
END
```

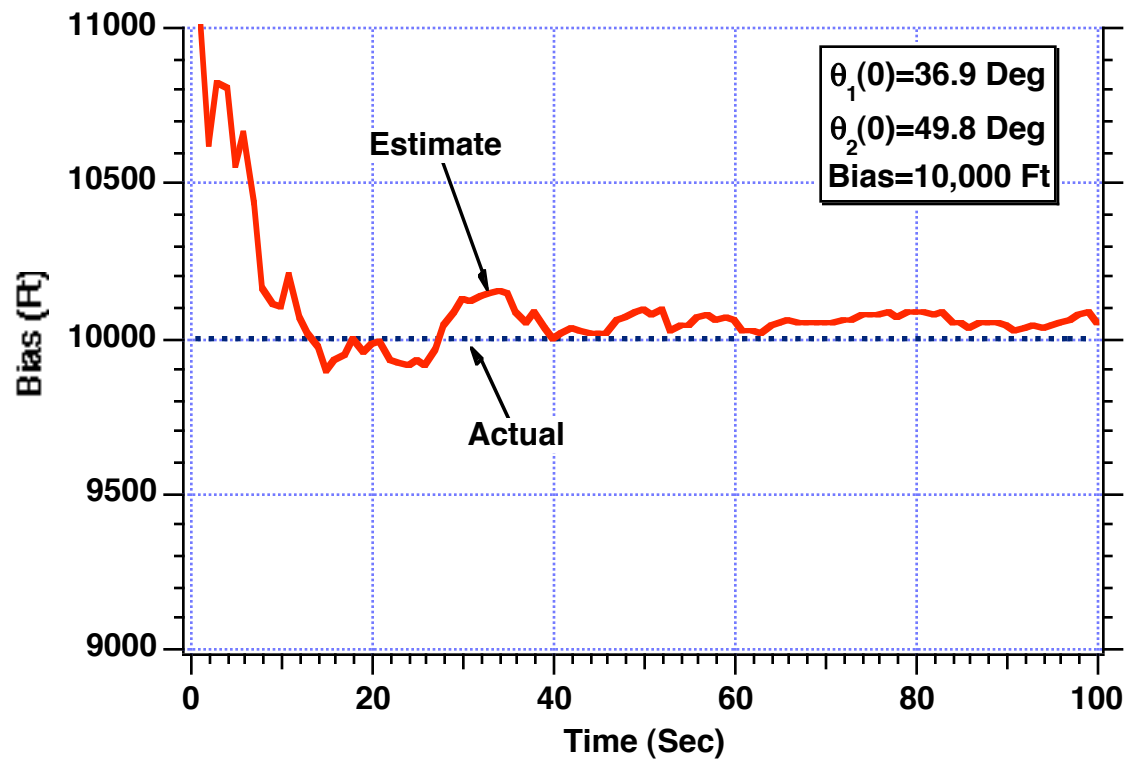
```
SUB GAUSS(X,SIG)
LET X=RND+RND+RND+RND+RND+RND-3
LET X=1.414*X*SIG
END SUB
```

Subroutine for zero mean Gaussian noise

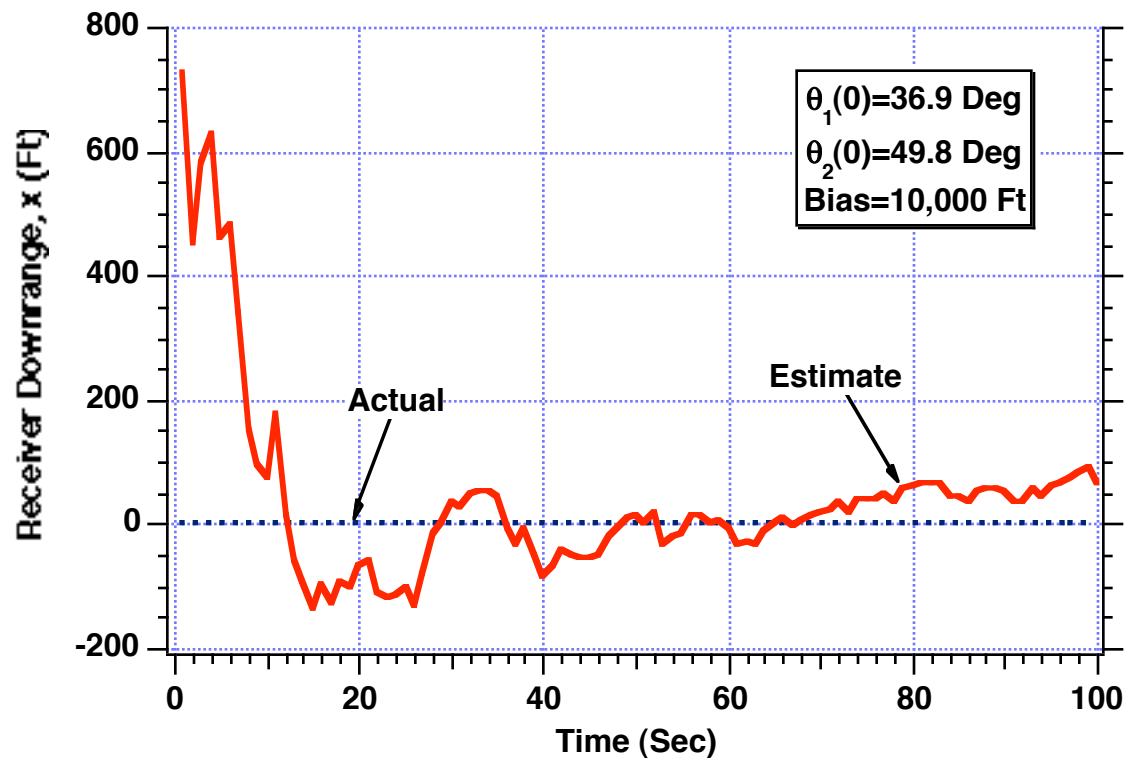
```
SUB ATAN2 (Y, X, Z)
IF X < 0 THEN
    IF Y < 0 THEN
        LET Z = ATN(Y / X) - 3.14159
    ELSE
        LET Z = ATN(Y / X) + 3.14159
    END IF
ELSE
    LET Z = ATN(Y / X)
END IF
END SUB
```

Arctangent subroutine which is good in all 4 quadrants

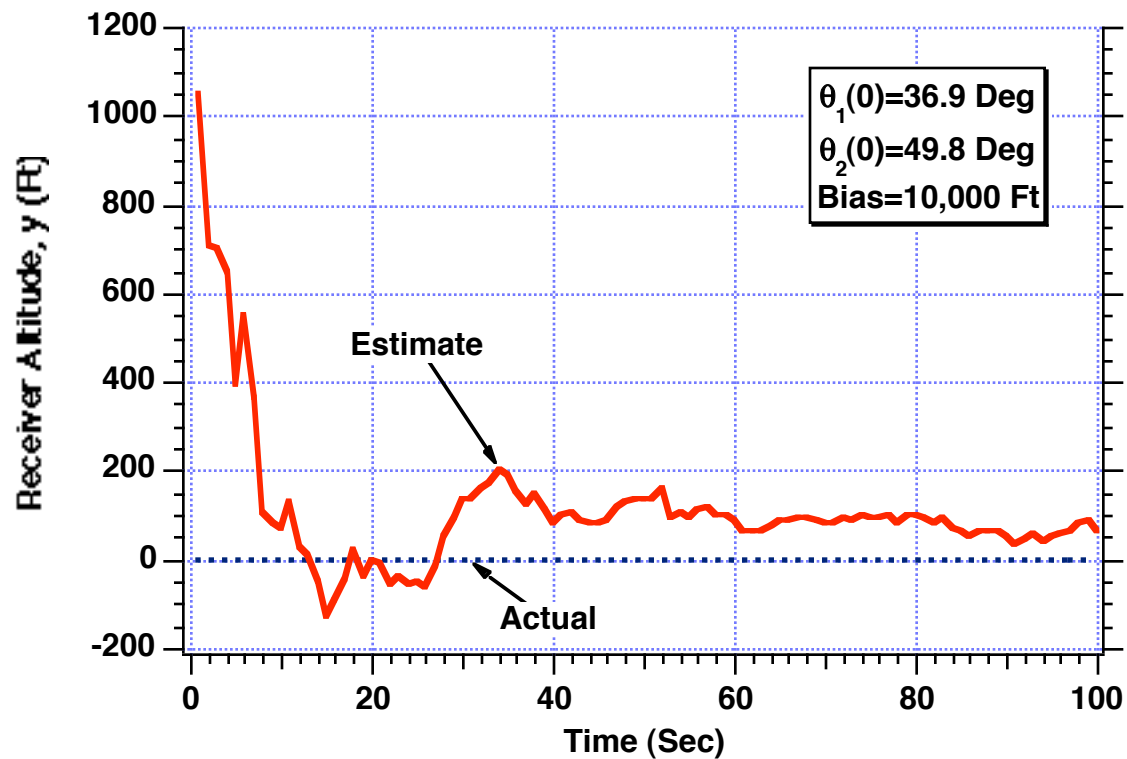
Three Satellite Range Measurements Enable New Extended Kalman Filter to Estimate Bias



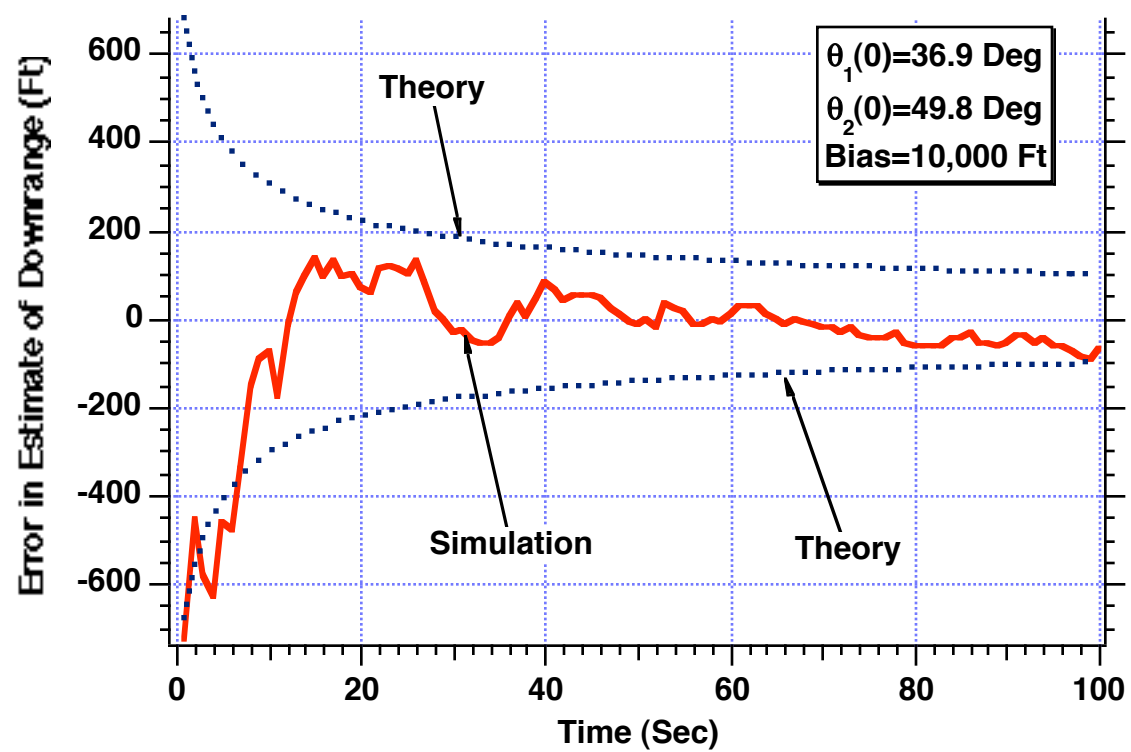
Three Satellite Range Measurements Enable New Extended Kalman Filter to Estimate Receiver Downrange



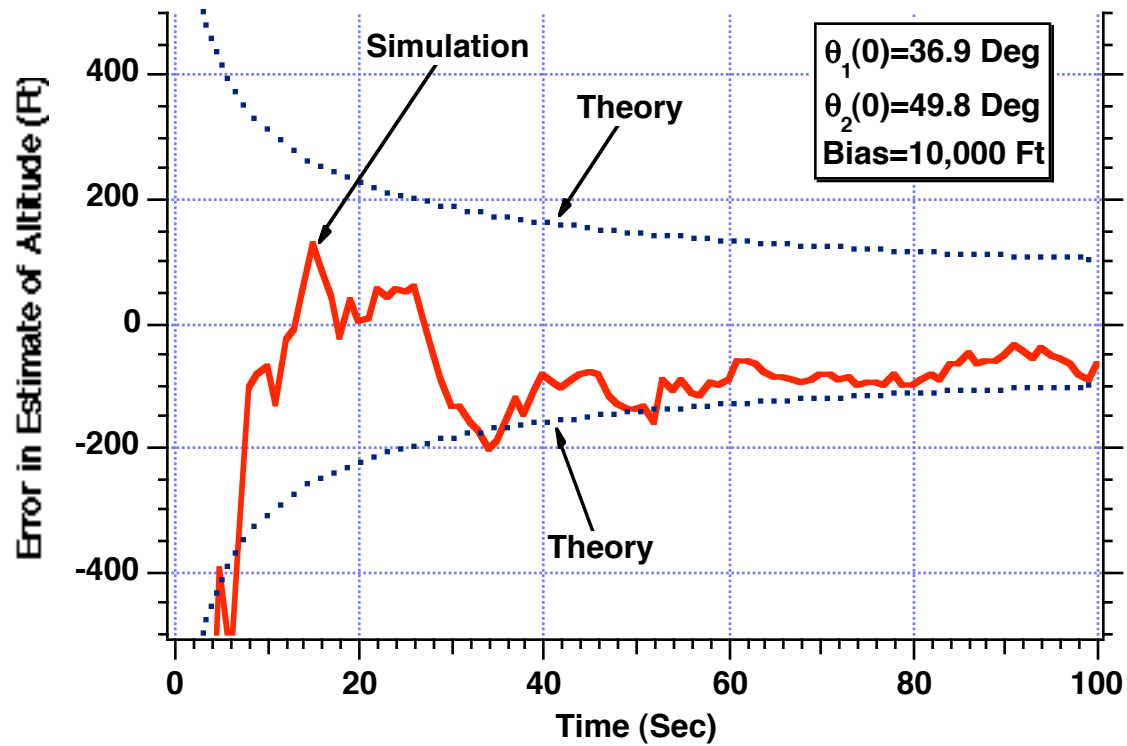
Three Satellite Range Measurements Enable New Extended Kalman Filter to Estimate Receiver Altitude



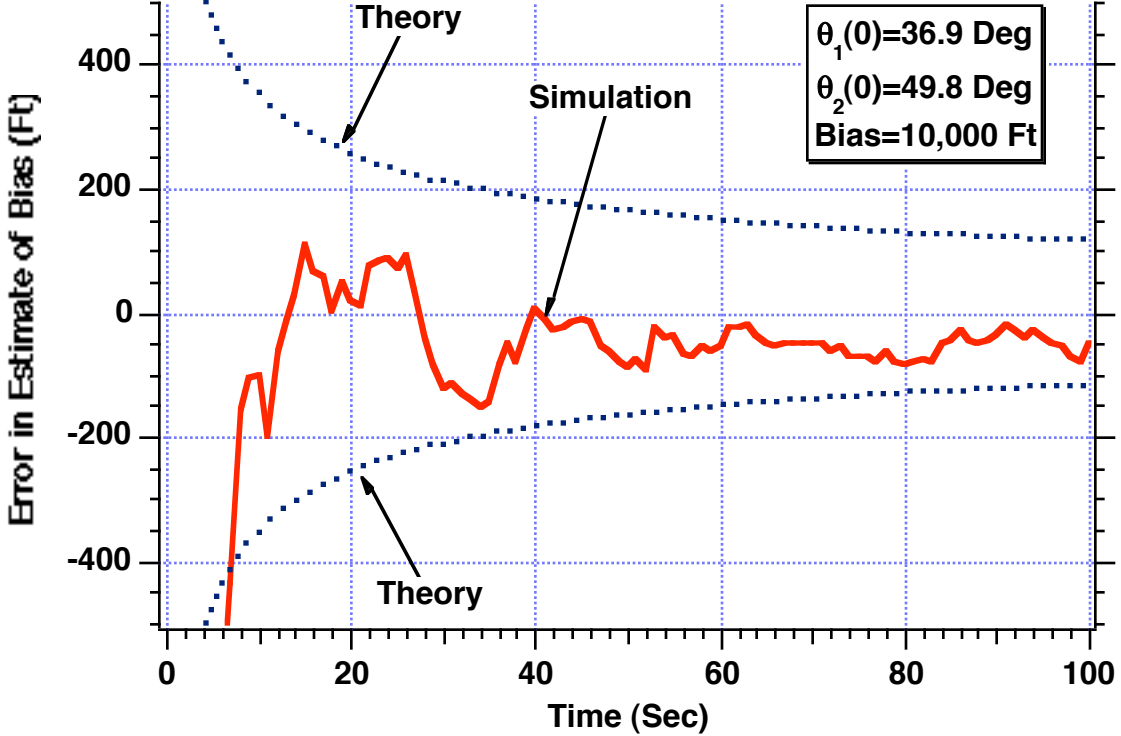
New Extended Kalman Filter Appears to be Yielding Correct Estimates of Receiver Downrange



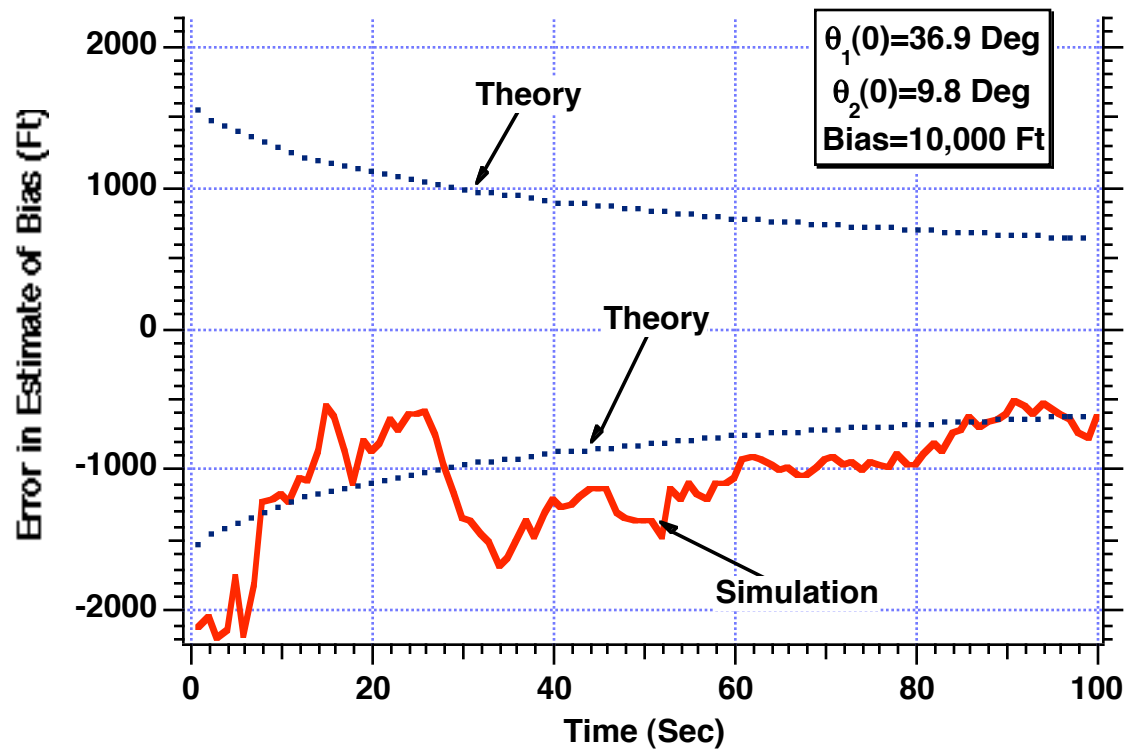
New Extended Kalman Filter Appears to be Yielding Correct Estimates of Receiver Altitude



New Extended Kalman Filter Appears to be Yielding Correct Estimates of Bias



Errors in the Estimate of Bias Get Larger as the Angle Between Second and Third Satellite Decreases



Biases Summary

- **If the satellite was causing the bias in the range measurement we could estimate the bias by taking range measurements from one satellite to a receiver whose location was known precisely**
- **If the receiver was causing the bias and the receiver location was unknown, three satellites were required in the two dimensional problem for an extended Kalman filter to estimate the bias and receiver location**