

Modelling Surface Wind for Ram-air Parachute Piloting Simulator

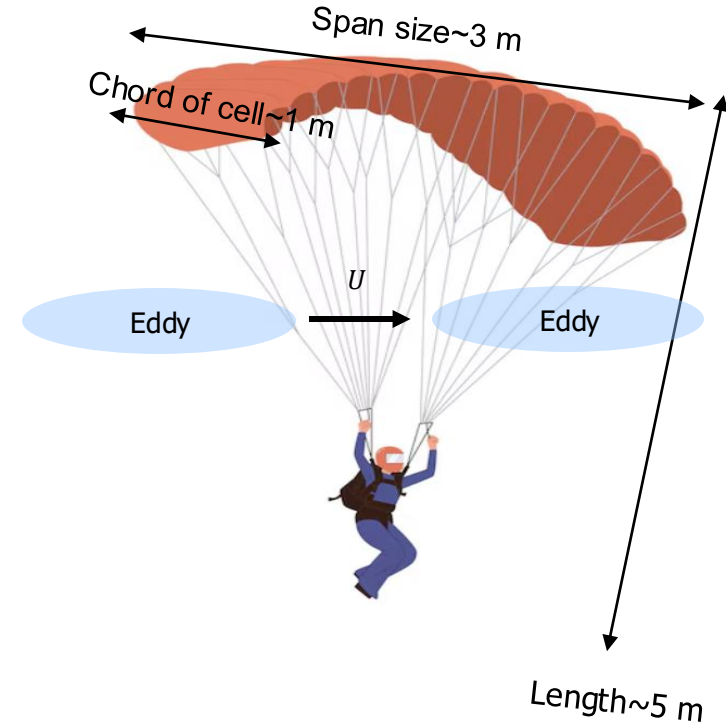
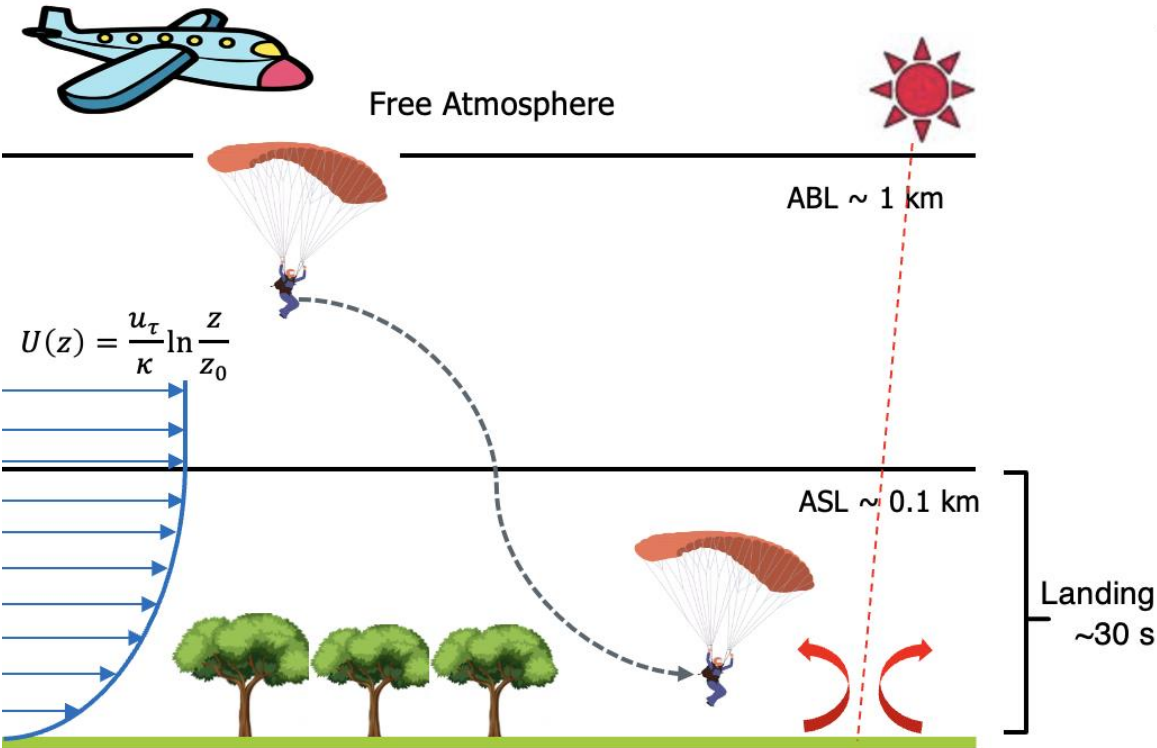
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Supervision by Dr. Anna Clarke and Prof. Ian Jacobi

Department of Aerospace Engineering, Technion

March 20, 2025

Flying Through the ASL



$$f = \frac{U}{\lambda} = \frac{10}{0.5} = 20 \text{ [Hz]}$$

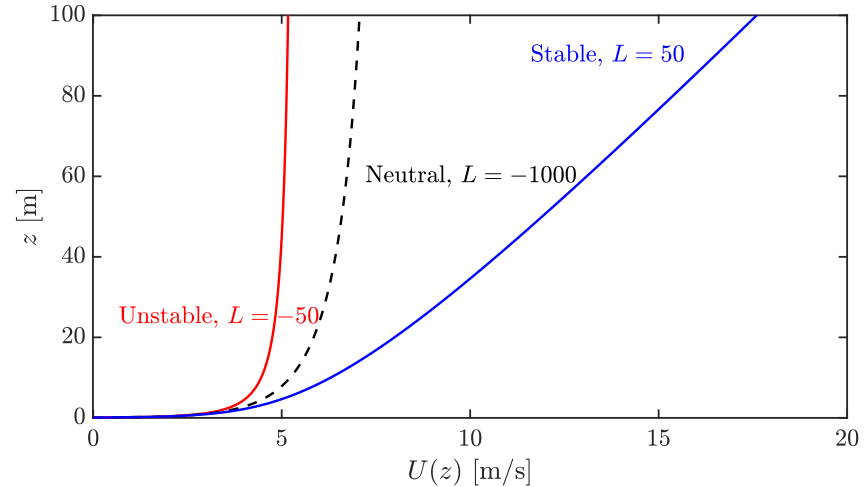
Modelling Mean Wind in the ASL

Mean velocity profile: $u = U + u$

$$-\infty < \zeta = \frac{z}{L} < \infty, L = \frac{-u_\tau^3 \bar{\theta}}{kg\bar{H}}$$

$$\frac{\kappa z}{u_\tau} \frac{dU}{dz} = \phi_m(\zeta)$$

$$\frac{\kappa z}{\bar{H}} \frac{d\theta}{dz} = \phi_h\left(\frac{z}{L}\right)$$

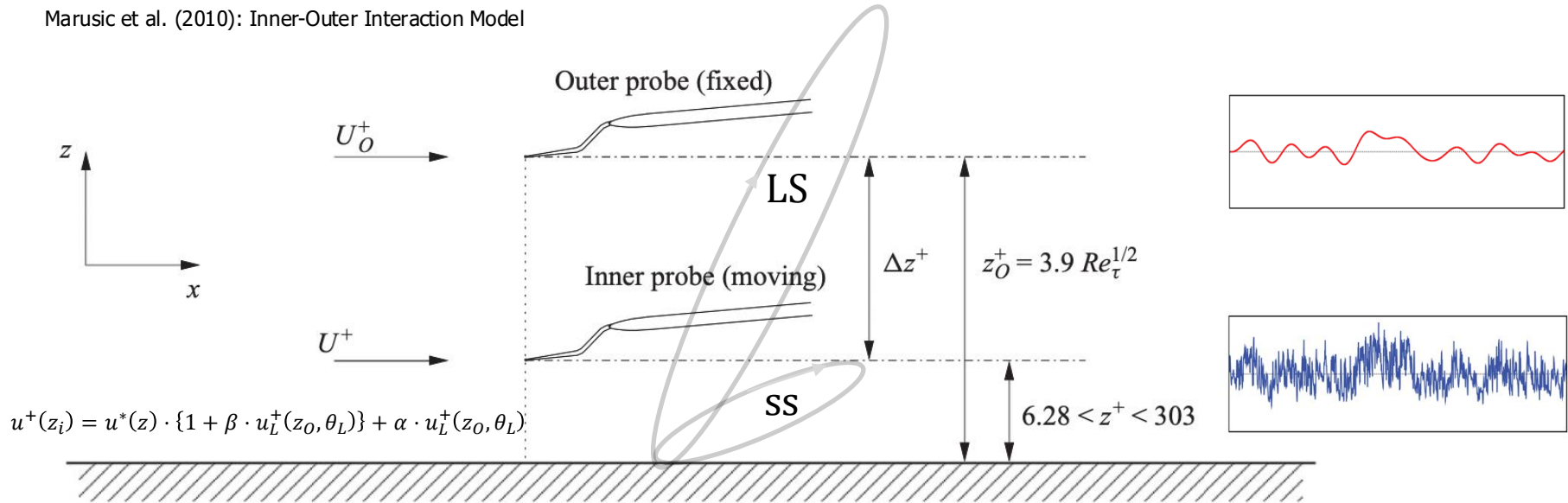


$\frac{z}{L} < 0$	$\frac{z}{L} > 0$	$\frac{z}{L} = 0$
$\phi_m\left(\frac{z}{L}\right) = \left(1 - \beta_m \frac{z}{L}\right)^{-1/4}$	$\phi_m\left(\frac{z}{L}\right) = 1 + \beta_m \frac{z}{L}$	$\phi_m\left(\frac{z}{L}\right) = 1$
$\phi_h\left(\frac{z}{L}\right) = \left(1 - \beta_h \frac{z}{L}\right)^{-1/2}$	$\phi_h\left(\frac{z}{L}\right) = 1 + \beta_h \frac{z}{L}$	$\phi_h\left(\frac{z}{L}\right) = 1$

Modelling Turbulence

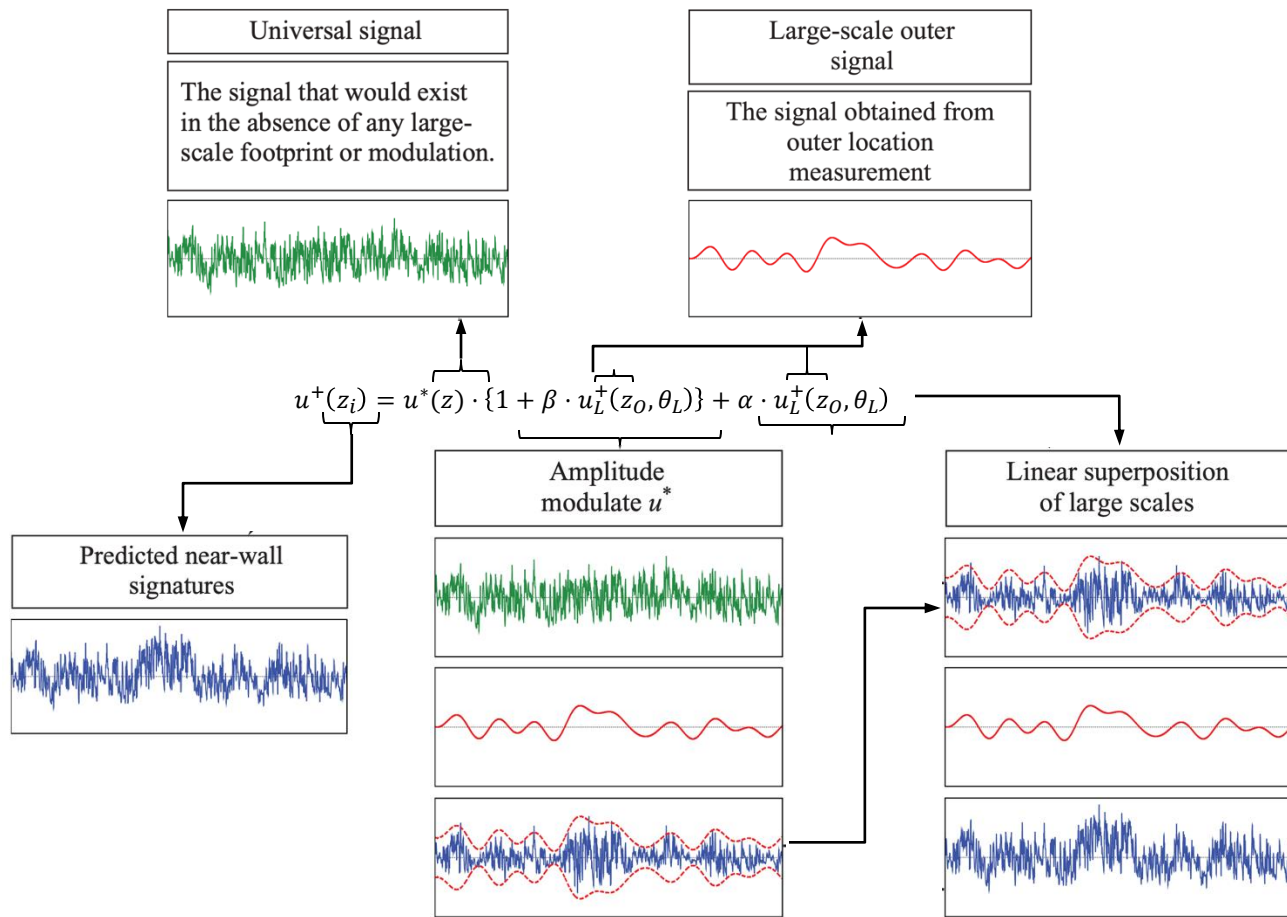
Higher order moments: $u = U + u$

Marusic et al. (2010): Inner-Outer Interaction Model

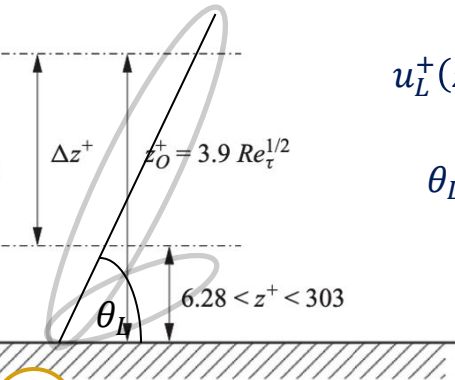
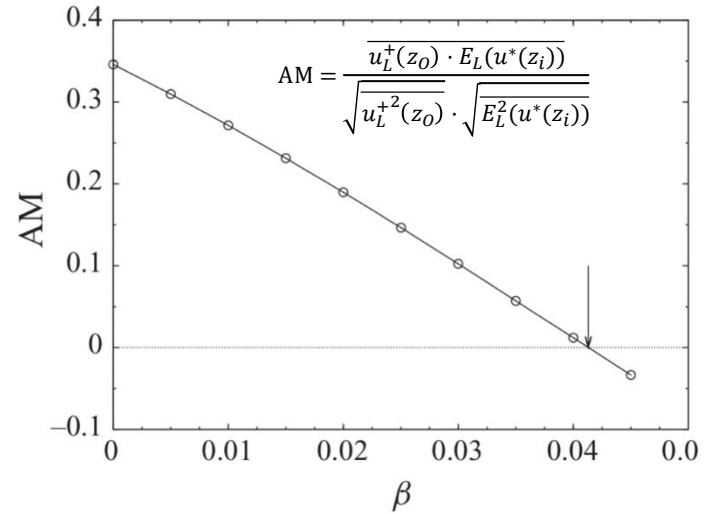
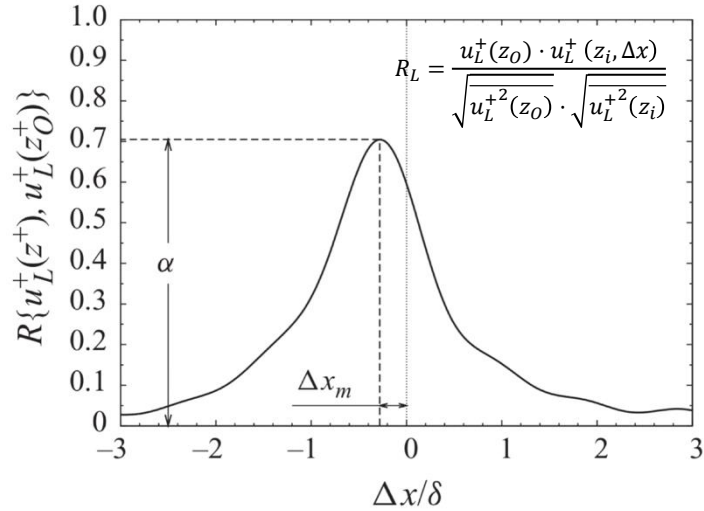


Inner-Outer Interaction Model

Mathis et al. (2011)



Parameters Determination



$$u_L^+(z_i) \approx \alpha \cdot u_L^+(z_0, \theta_L),$$

$$\theta_L = \arctan \frac{z_0 - z_i}{\Delta x_m}$$

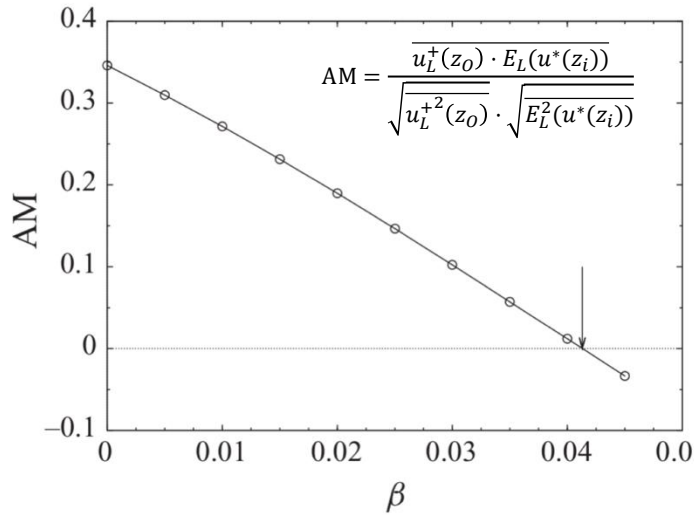
$$u^+(z_i) = \underbrace{u^*(z) \cdot \{1 + \beta \cdot u_L^+(z_0, \theta_L)\}}_{u_s^+} + \underbrace{\alpha \cdot u_L^+(z_0, \theta_L)}_{u_L^+}$$

$$u_s^+(z_i) \approx u^+(z_i) - \alpha \cdot u_L^+(z_0, \Delta x_m)$$

$$u^*(z_i) \approx \frac{u_s^+(z_i)}{1 + \beta \cdot u_L^+(z_0, \Delta x_m)}$$

$$AM(u^*(z_i)) = 0$$

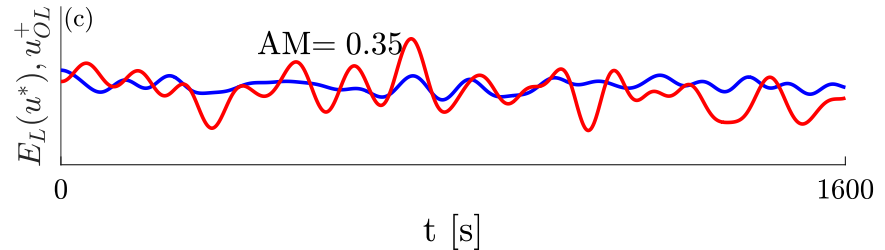
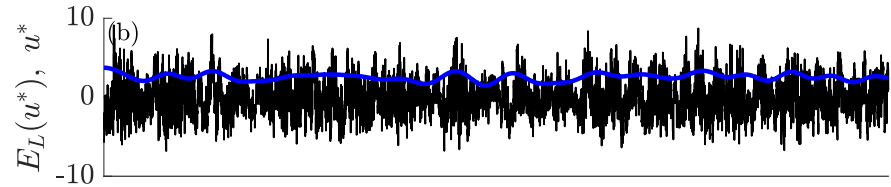
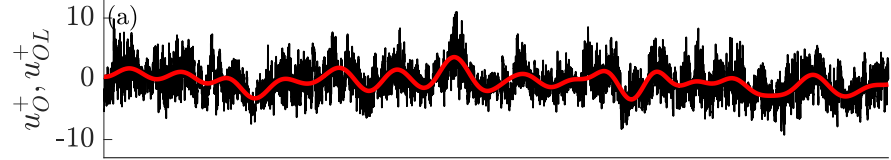
Parameters Determination



$$u_s^+(z_i) \approx u^+(z_i) - \alpha \cdot u_L^+(z_0, \Delta x_m)$$

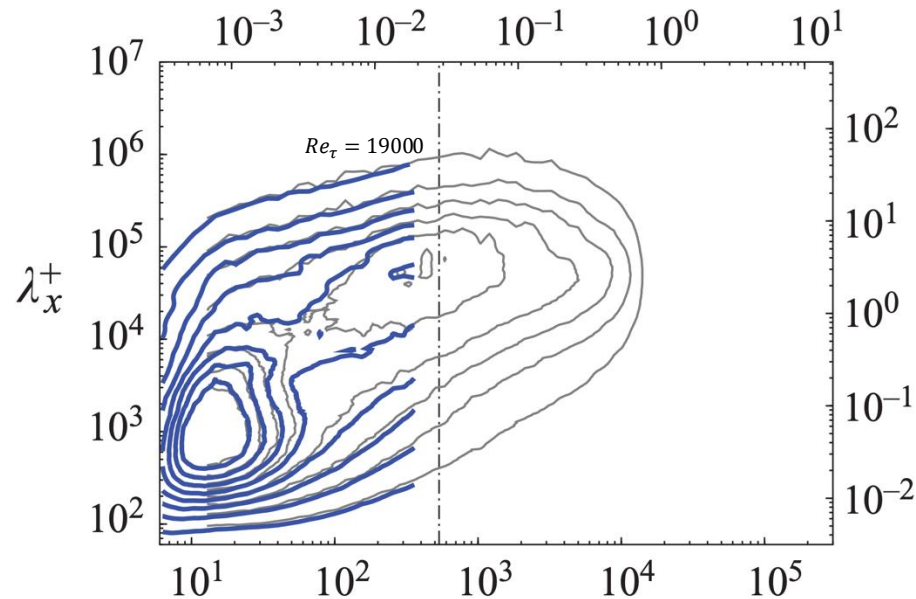
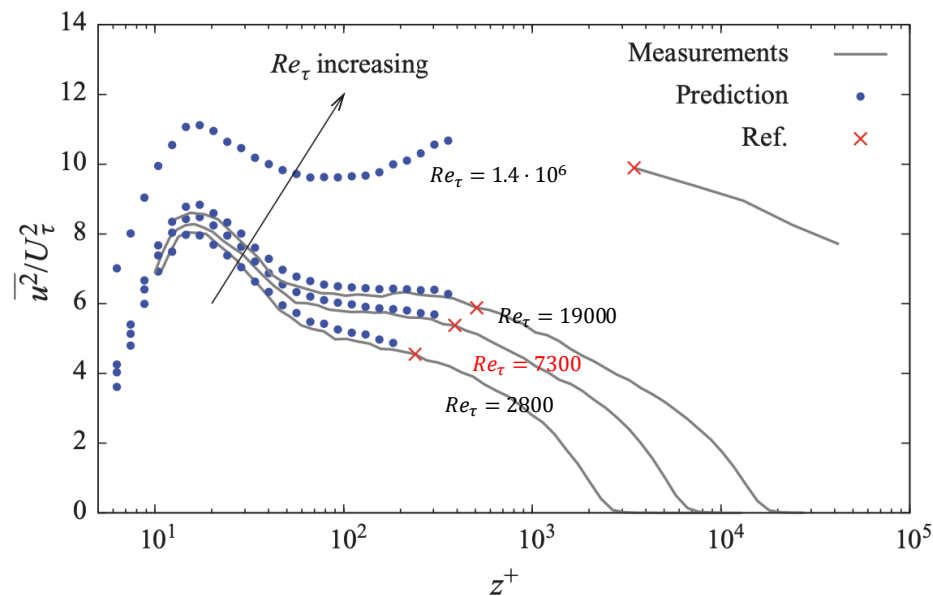
$$u^*(z_i) \approx \frac{u_s^+(z_i)}{1 + \beta \cdot u_L^+(z_0, \Delta x_m)}$$

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$$u^+(z_i) = \underbrace{u^*(z) \cdot \{1 + \beta \cdot u_L^+(z_0, \theta_L)\}}_{u_s^+} + \underbrace{\alpha \cdot u_L^+(z_0, \theta_L)}_{u_L^+}$$

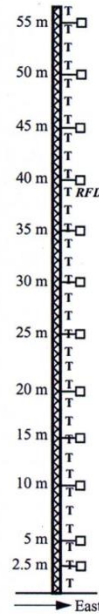
Inner Outer Interaction Model Predictions in Thermally Neutral Boundary Layers



$$Re_\tau = \frac{u_\tau \delta}{\nu}$$

Inner-Outer Model in the ASL

CASES99

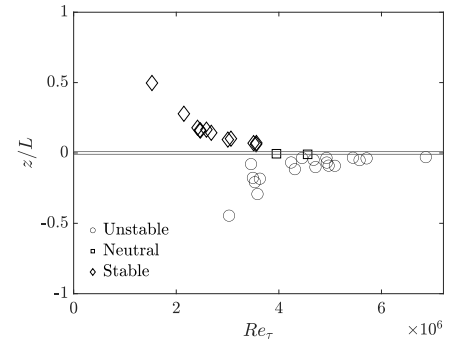
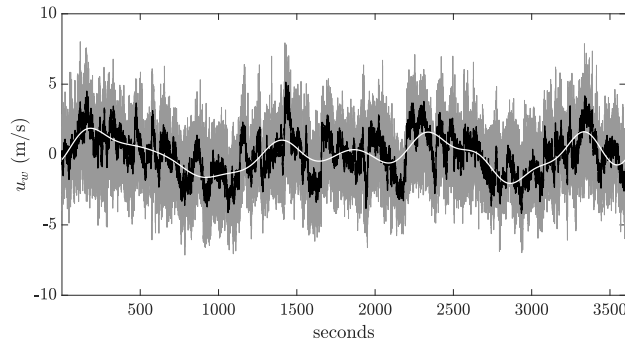


Measurements used:

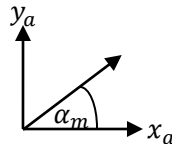
- u, v, w, θ 20 Hz, $z = 0.5, 5, 10, 20, 30, 40, 50, 55$ [m]

Processing stages:

- Hourly sections
- Dirction correction: $u_w = u_a \cos(\alpha_m) + v_a \sin(\alpha_m)$
- De-trending, $\delta = 150$ [m], $\lambda_{x, \text{detrending}} = 20\delta$
- $u_\tau = \overline{u_w w}$, $\frac{z}{L} = -\frac{zkg\overline{w\theta}}{u_\tau^3 \overline{\theta}}$, both calculated at $z = 5$ [m]
- Stationarity

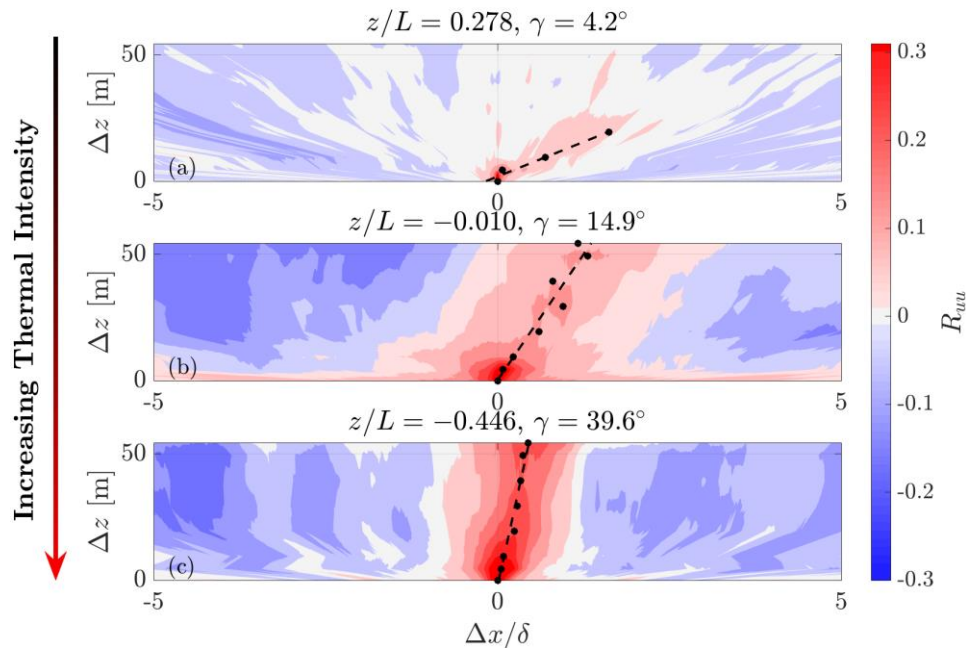
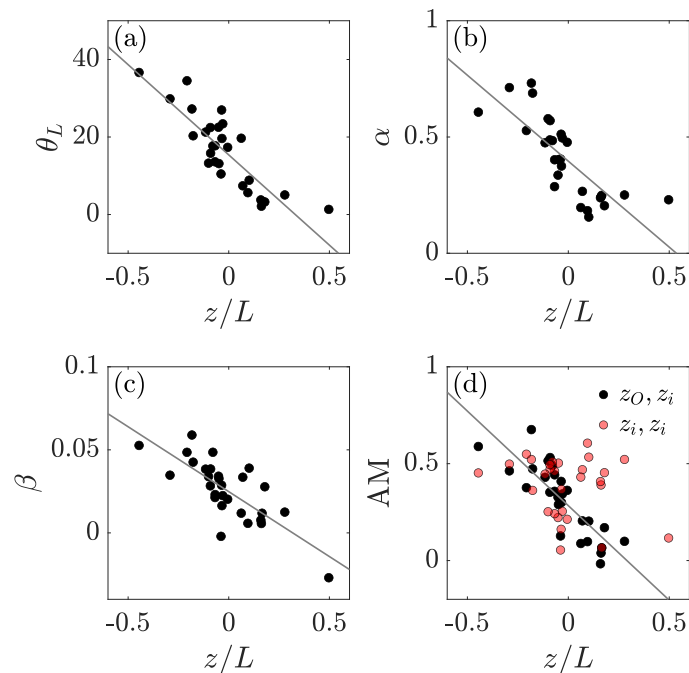


TOP VIEW



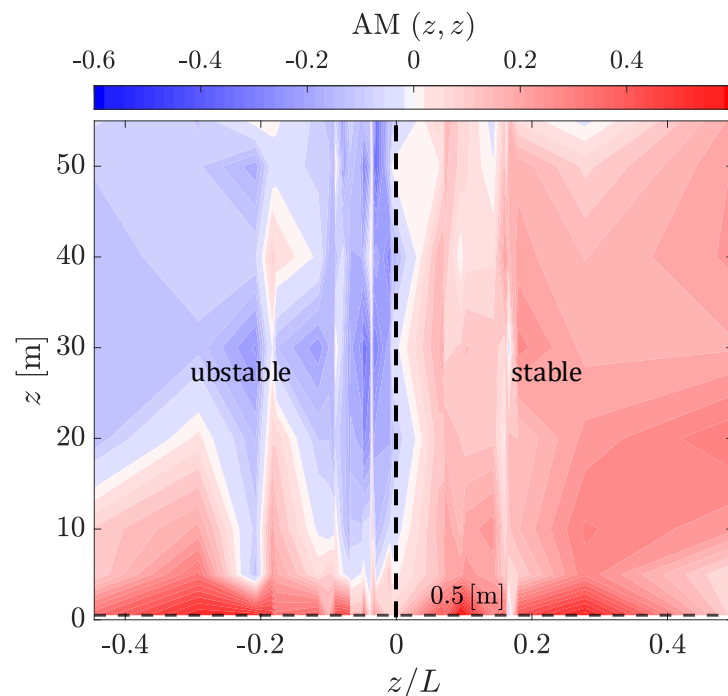
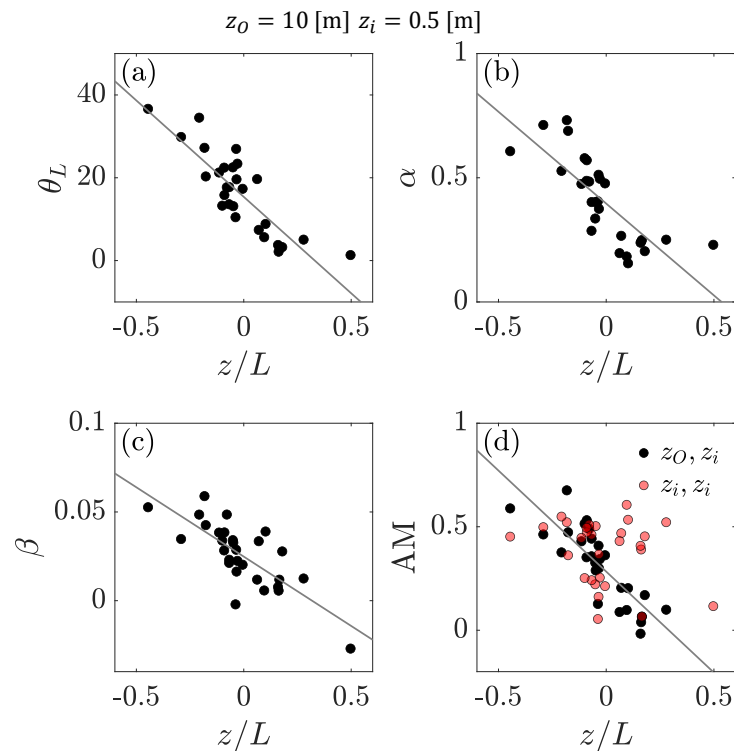
Stability Dependance of the Large-Scale Model Parameters

$z_0 = 10$ [m], $z_i = 0.5$ [m]



$$R_{uu} = \frac{u^+(z_0) \cdot u^+(z_i, \Delta x)}{\sqrt{u^{+2}(z_0)} \cdot \sqrt{u^{+2}(z_i)}}$$

Stability Dependence of the Small-Scale Model Parameters



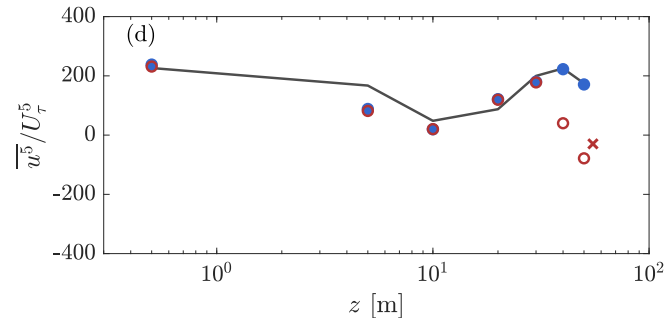
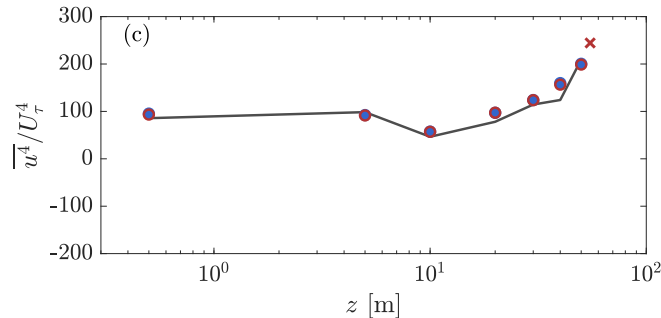
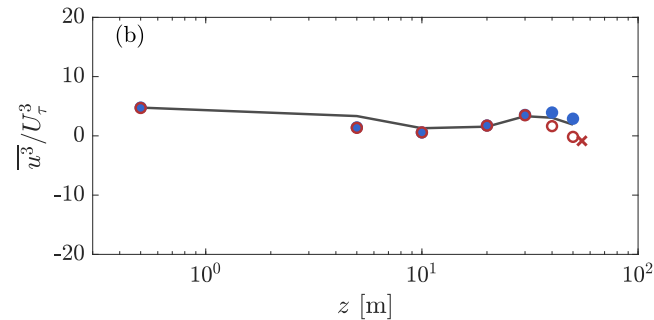
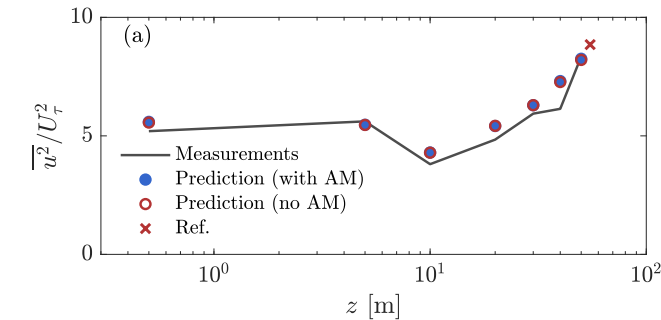
$$AM = \frac{\overline{u_L^+(z)} \cdot E_L(u_s(z))}{\sqrt{\overline{u_L^{+2}(z)}} \cdot \sqrt{E_L^2(u_s(z))}}$$

Prediction using the Inner-Outer Model- statistics

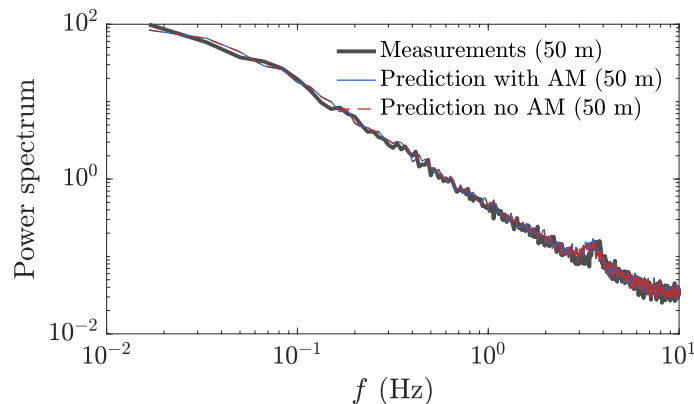
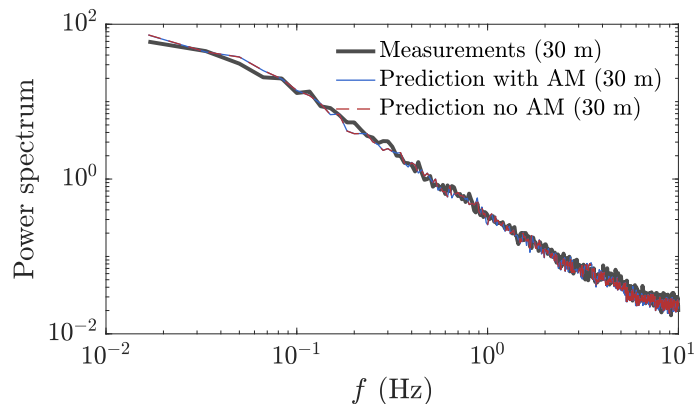
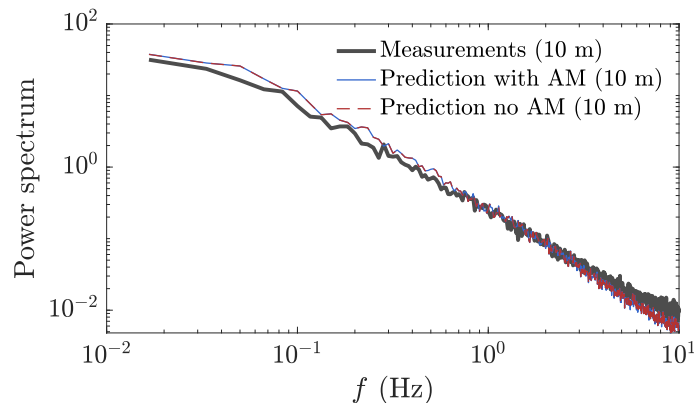
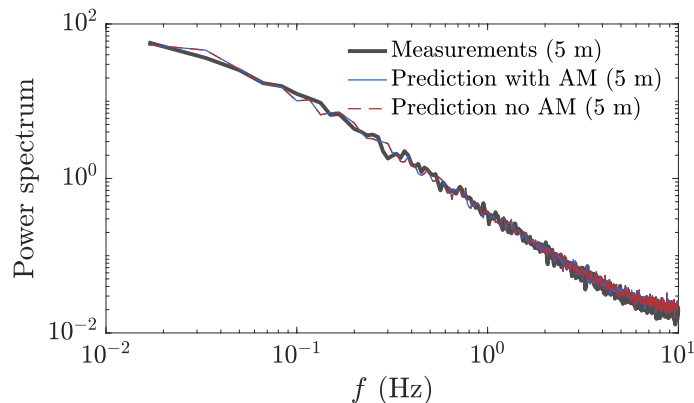
	Model parameters determination	Model validation
z/L	$0.159 \rightarrow \alpha, \beta, \theta, u^*$	0.162
Time and date (CST)	24-Oct-1999 22:00:00	27-Oct-1999 21:00:00

with AM: $u^+(z_i) = u^*(z) \cdot \{1 + \beta \cdot u_L^+(z_0, \theta_L)\} + \alpha \cdot u_L^+(z_0, \theta_L)$

no AM: $u^+(z_i) = u^*(z) \cdot \{1 + 0 \cdot u_L^+(z_0, \theta_L)\} + \alpha \cdot u_L^+(z_0, \theta_L)$

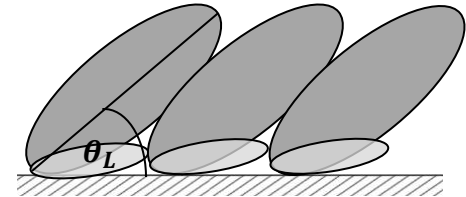
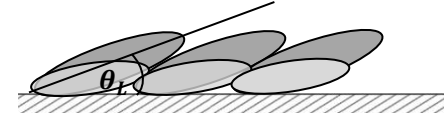


Prediction using the Inner-Outer Model- spectra



Conclusion

- Thermal stability affects the inner-outer model parameters. Stability suppresses mixing, limiting large-scale correlation.
- Spectra and moments up to fifth order are predicted well if the calibration signal have approximately the same stability condition.
- Amplitude modulation effect is expressed in the odd moments of turbulence.



Thank you!